

# Assessment of Geothermal Resources and Reserves in Denmark

A contribution to the geothermal resource  
and reserve estimate of the European  
Community



**DGU**

Geological Survey of Denmark

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A contribution to the geothermal resource  
and reserve estimate of the European  
Community

A DGU – EC project .

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## INTRODUCTION

### Project framework and objective

In 1979 the European Community (EC) Directorate-General for Research and Development invited the member states to look into the aspects of geothermal resource and reserve evaluation and practical implementation of the assessment exercise within the EC.

From fall 1979 to fall 1981 a working group, in which Denmark was represented by E. Gosk, set up guidelines for a description, classification, and evaluation of geothermal resources and reserves. The guidelines are basically those outlined by Muffler and Cataldi (1978), USGS Circ 790, and applied by Cataldi et al. (1978).

Contractors working on geothermal energy within the EC were from 1982 involved in the assessment of geothermal resources and reserves. From Denmark the company Danish Oil and Natural Gas A/S (D.O.N.G. A/S) and the Geological Survey of Denmark (DGU) were invited to participate in the assessment. D.O.N.G. A/S was involved as the company had the concession on geothermal energy in Denmark and was making exploration drilling. DGU was involved as the survey up to that date had made the regional mapping of the reservoirs (Michelsen et al. 1981) and was involved in contract work for the EC.

The contract (no. EG-B-3-005-DK(G)) between EC and DGU, 1981-1982, had the goal of investigating the reservoir properties of possible geothermal reservoir rocks. The study was terminated with the report "Geothermal Reservoirs in Denmark" (Priisholm et al. 1982).

The above mentioned contract was by a First Supplementary Agreement extended to cover 1983 with the aim of making an assessment of the geothermal resources and reserves in Denmark. The work is terminated with this final report.

The report is based on the general geological knowledge of the reservoir properties which are available at the survey from the previous studies and on data made available through the exploration activities of D.O.N.G. A/S. The evaluation of assessments has been carried out as a joint work where D.G.U. has contributed with the geology and reservoir data while Tage Sørensen A/S made the resource and reserve assessments.

## Contributors

S. Priisholm:                    Geology and reservoir data.

S. Christensen:                Resource and reserve assessment.

The geological part has been reviewed by L. Holm and suggestions to the resource and reserve assessment as well as major contributions to the appendices I & II has been made by G. Iversen (D.O.N.G. A/S). F. Larsen performed the planimetry of the areas.

Drafting was carried out by Kirsten Andersen, Eva Melskens and coordinated by Uli Jørgensen.

The typing was performed by Dorthe Plougmann.



## RESERVOIR DATA FOR ASSESSMENT

The guidelines for the assessment of geothermal resources and reserves are given by EC, DG XII, in working documents of 31 March 1980 and January 26th 1982. The documents are based on work by Muffler and Cataldi (1978).

The reservoir assessment require data and maps which gives

- I Lateral extend of each aquifer.
- II Isotherm map of each aquifer.
- III Net pay, porosity, permeability, transmissivity.

These and other relevant data are presented in the report by Priisholm et al. (1982) and the DONG A/S reports: "Undersøgelse af geologi, marked, teknik og økonomi for potentielle geotermiske anlæg i Midt- og Nordjylland". (July 1980) and "Undersøgelse af geologi, marked og økonomi for potentielle geotermiske anlæg i Sønderjylland og på Sjælland". (Febr. 1982).

Data and maps used for calculations are presented on figs. 1-10 and in tables 1-10 in this report.

A brief outline of parametre origin and trends as well as of the individual reservoirs are summarized in the following. Details are given in Priisholm et al. (1982).

## Definition and origin of parametres Table 1-5

### Reservoirs

The reservoirs drawn into consideration are the Bunter Sandstone Formation, Skagerrak Formation, Gassum Formation, Haldager Sand, and Frederikshavn Member (Fig. 3).

### Depth intervals

It has been convenient in the analysis to divide the reservoirs in 0,5 km thick sequences, as most reservoir parametres are depth dependent.

The individual depth sequences has been chosen from the maps shown on fig. 4-8.

### Regions

Within the 0,5 km thick depth sequences some of the reservoir parametres show lateral variation. Where this is the case the reservoirs have been divided into regions in order to limit these variations.

### Areas

The area of the regions has been measured using planimetry.

### Temperature

Temperature data are based on tabulations and maps presented in reports by Balling et al. (1981), Priisholm et al. (1982), and Saxov (1978).

These data have been interpolated using model A temperatures to give the average temperature at mean depth of the reservoir interval of a given region.

The determination of reserves does not alter with

moderate temperature variations, and hence only an average value is sufficient.

#### Porosity

By using the porosity versus depth plot of each reservoir (Fig. 9) and well data from a specific region the average porosity at mean depth of the reservoir interval has been calculated.

Moderate porosity variations does not alter the resource and reserve estimates, and hence an average value used.

#### Brine-permeability

Average, as well as minimum and maximum brine-permeability values for a certain reservoir interval are determined by using the correlation charts between porosity and depth, porosity and air-permeability (Fig. 10), and air- versus brine-permeability. Well data, including test results, and reservoir configuration has been taken into consideration.

The permeability parametre is critical in reserve analyses. Therefore and because the parametre is difficult to establish with certainty average as well as minimum and maximum values have been used.

#### Net reservoir thickness

Net thickness includes the sandstone layers which are considered to have reservoir quality and which could produce.

### Transmissivity

The productivity of the reservoir, the transmissivity, is the brine-permeability multiplied by net reservoir thickness.

The transmissivity is a very difficult value to measure or to calculate with certainty. The average, minimum, and maximum transmissivity has been estimated by using the brine-permeability, and the net sand thickness values as well as the knowledge from tests and sedimentological facies analyses.

## Outline of parametre trends

Parametres governing the reservoir characteristics and the performance of the reservoir rocks are the sedimentary environment, diagenesis, temperature-distribution, salinity, porosity, and permeability trends with increased depth.

### Sedimentary environment

In order to map the parametres of the sedimentary reservoir rocks, a classification into sedimentary environments has been carried out. In the interpretation this classification is important because the lateral reservoir extension, the net sand, porosity, and permeability are related to the type of sedimentary environment.

In general, the most high-energy environments, with the highest degree of reworking, have provided the most coarse-grained and well sorted sandstones.

The Haldager Sand and, to a lesser degree, the Skagerrak Formation, were both partly deposited in a braided river environment and are the most coarse-grained sediments of the investigated formations. This environment can provide sandstone bodies of considerable extension.

The Gassum Formation was deposited in a tidally influenced, shallow marine platform environment. The coarse-grained fraction of the Gassum Formation (fine- to medium-grained sand), is finer-grained than the above-mentioned sediments and was deposited under intermediate energy conditions.

The Frederikshavn Member was probably deposited in an near-shore intermediate-energy environment also, but no obvious relationship between energy levels and grain size can be determined.

The lowest-energy environment in general of the discussed formations is the sabkha regime which is exemplified by the Bunter Sandstone Formation and provides the most fine-grained sandstones.

#### Diagenesis

The degree of diagenesis of the reservoir is important to know in order to evaluate the porosity and permeability. It has been evaluated with the aid of thin sections, x-ray, SEM, and heavy mineral studies.

The Bunter Sandstone and Skagerrak Formations have suffered redbed diagenesis with the formation of hematite, authigenic feldspar, and carbonates. The Skagerrak Formation, when containing easily dissolvable volcanic material, have especially strong diagenetic effects which resulted in lower porosity.

The Gassum Formation becomes increasingly cemented with increasing temperature (depth). Dissolution of feldspars at greater depths creates secondary porosity.

The Haldager Sand has no important early cementation and thus suffers great compaction (crushing of grains) at deep levels. The Frederikshavn Member has a very early glauconitic cement which, combined with the matrix, lowers the permeability considerably.

### Temperature

Isotherm maps of each formation and at depth of 2000 m and 3000 m have been constructed.

Isolines generally follow the main tectonic units; the highest temperatures are predicted for the central Danish Subbasin with temperatures decreasing NE towards the Fennoscandian Border Zone and SE towards the Ringkøbing-Fyn High, above, and within which, the lowest temperatures are predicted.

Temperatures range between 55 degree C and 75 degree C at 2000 m depth, and between 75 degree C and 105 degree C at 3000 m depth. In the deepest part of the Skagerrak Formation in the Danish Subbasin, temperatures may reach 100-150 degree C.

### Salinity

The formation water data have been obtained from tests and from extraction of interstitial waters in cores.

The salinity of the formations-waters in question shows an almost linear increase in salinity with depth. The major solutes are sodium-, calcium-, magnesium-, and potassium chloride. The ions found in minor concentrations are bromide, strontium, sulfate, and bicarbonate.

Analyses have shown an increase in the calcium to chloride ratio with depth, and a narrow range of the bromide to chloride ratios. This indicates a common origin of the post-Zechstein formation waters.

The Salinity increase is interpreted as due to filtration of the interstitial waters through semipermeable membranes, which allow only H<sub>2</sub>O and some of the ions to pass through. As the compaction of the sediments proceed, the interstitial water will be progressively more concentrated.

#### Depth, porosity, and permeability

Despite the great differences in sedimentary environments, diagenesis, and porosity/permeability values of the reservoirs, and bearing in mind the limitation in data on which the gradients and trends are based, the geothermal reservoirs in Denmark, as known today, have characteristics which fall within broad bands with a common decrease in porosity with depth. The porosity band is from 30-40% porosity at about 500 m depth to 5-15% at about 3500 m depth, and the brine-permeability is in the range 300-3000 mD at about 30% porosity decreasing to 10-30 mD at 15% porosity. Most likely, the reservoir values will fall, within these broad trends. The analyses presented for each reservoir indicate that the reservoir potential at depths below 2500 m is low.

#### Depth versus porosity Fig. 9

The different depth versus porosity trends of the geothermal reservoirs can be illustrated by the variations in porosity gradients which are 5% per 1000 m for the Skagerrak Formation, 9% per 1000 m for the Gassum Formation, 8% per 1000 m for the Haldager Sand and 9% per 1000 m for the Frederikshavn Member. No gradients are established for the Bunter Sandstone Formation.



A comparison between the linear regression trends of the geothermal reservoirs shows that the Frederikshavn Member, Haldager Sand, and Gassum Formations have almost the same linear decrease of porosity with depth (Fig. 9), from about 35% porosity at 500 m to 10-15% at 3000 m. The data from the Bunter Sandstone Formation have no porosity/depth trend, but the data clouds of the formation fall within the stated trends; about 30% at 1000 m and 25% at 1500 m.

The linear trend and porosity gradient of the Skagerrak Formation indicates a less drastic decrease in porosity with depth compared to the above-mentioned trend. The decrease is from about 20-25% porosity at 1500 m to 0-10% at 5000 m. The lower gradient of the Skagerrak Formation cause the trend line of this formation to cross the other trend lines at 2000-2500 m depth. Consequently, the porosity of the Skagerrak Formation is lower than for the other reservoirs at a given depth above 2000 m, whereas the porosity of the Skagerrak Formation is higher below 2500 m. In the range 2000-2500 m, all reservoirs have porosities of 15-25%.

Porosity versus permeability Fig. 10

The porosity/air-permeability trends established for each geothermal reservoir are compared in fig. 10. They have almost the same linear trend from 40 mD permeability at 15-18% porosity down to 1 mD at 2-4% porosity. Above 40 mD at 15-18% porosity, the Skagerrak Formation and Haldager Sand have a common, "high permeability" trend with 2000 mD air-permeability at 30% porosity, whereas the Gassum and Bunter Sandstone Formations have a trend predicting 2000 mD air-permeability at 35% porosity.

Using these trends together with the depth/porosity relations, a rough indication would be that 40 mD permeability is found at 2500 m depth and, for a given depth above 2500 m, the Haldager Sand and Skagerrak Formation will have higher air-permeability (almost a factor two higher) than the Gassum and Bunter Sandstone Formations. In the Bunter Sandstone and Skagerrak Formations the analysis of the reduction going from air- to brine-permeability is found to be in the range of 50%.

For the Gassum Formation and the Haldager Sand the decrease from air- to brine-permeability is negligible above 1000 mD. At 1000 mD air-permeability the reduction is 30% for the Gassum Formation and 25% for the Haldager Sand. Near 100 mD the reduction is 50% for both reservoirs.

If the sedimentary environment, diagenesis, depth/porosity and porosity/permeability relationships are considered as a whole, it may be concluded that the relatively high-energy Haldager Sand and Skagerrak Formation, have similar porosity/high permeability trends although they differ in diagenetic history and, in certain localities, in lithology. This may cause the differences in porosity gradients where the Haldager Sand has high porosities at shallow depth of burial compared to the Skagerrak Formation (Fig. 10). With a reduction of 25-35% from air- to brine-permeability for the Haldager Sand, compared to 50% for the Skagerrak Formation, the properties of the Haldager Sand are the most favorable of these two reservoirs. The Skagerrak Formation however, has a much greater net sand thickness but it also has a province of volcanic materials resulting in extensive diagenesis causing low reservoir quality.

Of the formations deposited in moderate to low energy environments, a porosity gradient can only be established for the Gassum Formation. A similar trend could be expected for the Bunter Sandstone Formation. The porosity/air-permeability trends for the Gassum and Bunter Sandstone Formations are similar but a difference is noted in air- to brine-permeability reduction with better reservoir properties in the Gassum Formation.

Although the porosity gradient of the Frederikshavn Member follows the general trend as shown in fig. 9, the very early cementation is indicated by the porosity/low permeability trend.

#### General outline of geothermal reservoirs

Based on the report "Geothermal Reservoirs in Denmark" a general outline of the geothermal reservoirs in Denmark can be given.

Regional description of the rocks are previously published by Bertelsen (1978 and 1980), Larsen (1966), and Michelsen (1978 and 1981).

The possible reservoirs considered here are the Lower Triassic Bunter Sandstone Formation in the North German Basin, and the Lower to Upper Triassic Skagerrak Formation, Upper Triassic Gassum Formation, the Middle Jurassic Haldager Sand, and the Upper Jurassic to Lower Cretaceous Frederikshavn Member, situated in the Danish Subbasin (Fig. 3).

The structural elements of Denmark are presented in fig. 2 while the configuration of the Triassic formations is given by the general isopach map of the total Triassic (Fig. 5), and the depth map to near top Triassic (Fig.6). General depth maps of the Gassum Formation, Haldager Sand, and Frederikshavn Member are presented in fig. 6-8 .

#### Bunter Sandstone Formation

In the southern and southwestern part of southern Jylland, transmissivities are probably in the range of 5 to 25 Darcymetres. In the troughs, the formation is thicker and the transmissivity is hence expected to be high. The reservoir bodies may be characterized as sheet with a possible great areal extension, measured in kilometres of width. The temperatures are 50-70 degrees C. On Lolland-Falster, the temperatures are lower (about 40 degrees C) because of a more elevated shallow position of the formation. The northern boundary of North German Basin, as defined by the Ringkøbing-Fyn High, may be a reservoir area because of the increasing sandy content with approach to Skagerrak Formation further to the north. Temperatures north of the Ringkøbing-Fyn High on Sjælland are 50-70 degrees C.

#### Skagerrak Formation

In areas where the formation is situated above 2000-2500 m depth, and where the depositional environment is the braided river regime with extensive sand bodies, transmissivities may be in the order of 20 Darcymetres.

In the central part of the Danish Subbasin, the formation is situated more deeply and thus has a lower permeability, except above salt pillows where the transmissivity may be high. Further, positive temperature anomalies can be present above the salt structures. A westerly province with the volcanic materials will have reduced transmissivities.

In North and Middle Jylland transmissivities may reach the order of 25-50 Darcymetres and at shallow depth, 1000-1500 m, in North Jylland 50-75 Darcymetres can be encountered locally.

In the Fennoscandian Border Zone (North Jylland), the depositional environment is dominated by alluvial fan deposits which generally are poorly sorted and thus the permeability will be lower. Sand body extension is probably relatively small measured in hundreds of metres.

In general, the estimates of the Skagerrak Formation are questionable because of few data.

#### Gassum Formation Fig. 6

In areas where the formation is situated shallower than 2000 m depth, and where net sand is relatively thick, transmissivities may be in the order of 10-20 Darcymetres or even higher. In most of the Ålborg Graben and in parts of Mid-Sjælland, these conditions should be fulfilled. The temperatures are 40-70 degrees C here. In addition, areas above salt structures in the central part of the Danish Subbasin may have similar reservoir properties (e.g. Thisted structure, more than 100 Darcymetres).

In the deeper part of the Danish Subbasin, down to 3000 m, transmissivities are 0.5-5 Darcymetres and temperatures are 60-100 degrees C. The depositional environment is the shallow marine platform, in which the sandstone bodies most common will have an extent within hundreds of metres but they may coalesce to form bodies of greater extent.

On Lolland-Falster, net sand thicknesses of 50-70 m are found. The depth to the formation is 500-700 m here, and the temperatures are 20-30 degrees C. An estimate of other reservoir properties can not be given for this region at the present time because of lack of sufficient data, but high transmissivities, in the order of 50 Darcymetres may be expected.

#### Haldager Sand Fig. 7

In areas where the member is deposited as relatively extensive sand bodies in a braided river environment and where it is situated at depths less than 2000 m, transmissivities may be in the order of 10-20 Darcymetres. The net sand thickness is, however, expected to vary locally. The above-mentioned conditions are probably present in the Ålborg Graben, especially in the southern part where the braided river environment dominates. Further, in relation to salt structures in the central part of the Danish Subbasin, transmissivities may be high. The transmissivity elsewhere in the area is possibly around 5 Darcymetres. Temperatures in the Ålborg Graben are 40-60 degrees C, and 60-80 degrees C in the central part of the Danish Subbasin.

Frederikshavn Member Fig. 8

In the Fennoscandian Border Zone in Jylland, in the Ålborg Graben and in the easternmost part of Jylland, transmissivities may be in the order of 10-20 Darcymetres. The lateral extension of the sand bodies may be relatively large. Temperatures of the member are 20-40 degrees C in northern Jylland and 50 degrees C in the eastern part of Jylland. Due to the poor quality of the material however, the estimates of the transmissivity are uncertain and the postulated values may be too high.

## RESOURCE AND RESERVE ASSESSMENT

The guidelines for the assessment of geothermal resources and reserves are given by EC, DG XII, in working documents of March 31st 1980 and January 26th 1982. The documents are based on work by Muffler and Cataldi (1978).

As only low-enthalpy geothermal resources are found in the Danish sedimentary basins, the evaluation procedure is reduced to what is outlined in fig. 11. Corresponding definitions, formulae and nomenclature are found below (see also Fig. 12).

### Definitions and formulae

The following definitions and formulae are those valid for low-enthalpy geothermal reservoirs.

#### Accessible Resource Base (ARB)

(ARB) is the heat stored in rocks and fluids below a specific area down to a depth (7 km) accessible by current drilling technology and practice and measured as the temperature rise from mean (annual) ground temperature to actual temperature at depth. Per unit area ARB is expressed as:

$$(1) \quad ARB = \int_0^h C_t(h) \times (T(h) - T(h=0)) \times dh.$$

where  $C_t(h)$  is the total heat capacity in the reservoir at depth  $h$ .

$T_D(h)$  is the temperature at depth  $h$ .

$T(h=0)$  is the local mean annual ground temperature.

A detailed description is given in appendix II.



The total heat capacity of the reservoir (rocks and fluids) is found as:

$$(2) \quad C_t(h) = \phi(h) \times C_w(h) + (1 - \phi(h)) C_r(h)$$

where  $\phi(h)$  is the reservoir effective porosity at depth  $h$ .

$C_w(h)$  is the fluid heat capacity at depth  $h$ .

$C_r(h)$  is the rock heat capacity at depth  $h$ .

For more detailed analyses please refer to appendix I.

#### Geothermal Resource (GRSCE)

GRSCE is the heat or/and energy in place stored in a reservoir volume characterized by exploration evidence and which could be produced at some future time. All actual reservoirs can be characterized as low enthalpy Hot Wet Rocks (HWR) (low enthalpy reservoirs are hot water reservoirs with a temperature below 150 degrees C). According to this fact, the HWR resources in the actual case only consists of Heat in Place (HIP).

### Heat in Place (HIP)

Per unit reservoir volume HIP is equal to the sum of heat stored in the host rock and in the fluid, assuming thermal equilibrium and measured from the mean annual ground temperature, e.g.:

$$(3) \text{ HIP} = C_t \times (\bar{T} - T_0)$$

where  $C_t$  is the total heat capacity in the reservoir.

$\bar{T}$  is the mean temperature in the reservoir.

$T_0$  is the local mean annual ground temperature.

### Identified Resources (IR)

IR represents that part of the geothermal resources economically and legally produceable at some specified time in the future. For a low enthalpy hot water system IR can be written (per unit volume)

$$(4) \text{ IR} = \text{RHW MAX} \times \text{HIP where}$$

RHW MAX (Max. Recovery Factor) gives the ratio of the entire amount of energy in a reservoir (HIP) which is practically extractable (IR). For a doublet practical experience in France has shown, that RHW MAX can be calculated as (see Lavigne 1978):

$$(5) \text{ RHW MAX} = 0.33 \times \frac{\bar{T} - 25^\circ\text{C}}{\bar{T} - 8^\circ\text{C}}$$

See also formula (7).

### Identified Reserves (IRSVE)

IRSVE is the gain in energy when exploiting the identified, geothermal resources. This is expressed by a recovery factor RHW, which is difficult to determine. The factor depends on the site specified geological conditions as well as on the costs of installation and operation of heating plant and distribution system. According to the calculations made by Wurtz in Michelsen et al. 1980 RHW is roughly estimated to be 50%. IRSVE is then found to

$$(6) \text{ IRSVE} = 0.5 \times \text{IR}$$

IRSVE (or parts of it) is characterized as either proven, probable or possible reserves.

Proven Reserves represents that part of IRSVE which is supported by geological and drilling evidence (e.g. direct assessment) at the time of determination.

Probable Reserves represents that part of IRSVE which is based on geological, geophysical and/or geochemical (but not local drilling) evidence at the time of determination.

Possible Reserves represents that part of IRSVE which is based only on geological evidence at the time of determination.

## Discussion of parametres

### Accessible Resource Base (ARB)

ARB is a theoretical estimate of the geothermal heat, that could be available with the current drilling technology. Despite ARB represents the heat stored down to a depth of 7 km, it is today only technically and economically feasible to exploit the part stored above 3 km depth. According to calculations in Appendix II this forms a 25% of the total ARB.

The practical relevance of the determination of ARB is moderate compared with the relevance of the determination of the identified geothermal reserves, that today or in the near future can be exploited. For that reason ARB is only calculated for a typical, geological profile from the central part of the Danish Subbasin. The variation in relevant parametres above a depth of 7 km, is limited and the calculated order of magnitude of ARB is considered as typical for the entire Danish area. The value therefore can be used to compare the future possibilities of geothermal energy exploitation in Denmark and other European countries.

Calculating ARB it is assumed, that the temperature gradient from the surface to a depth of 3150 m is constantly 0.028 degrees C/m. Below this depth the temperature gradient is assumed to be 0.020 degrees C/m. This simplification introduces an uncertainty on ARB, that is considered less than 10%. That the sensitivity of ARB to temperature variations is moderate, is illustrated by a calculation with a constant temperature gradient of 0.024 degrees C/m. The difference between the two results is less than 6%.

In Appendix I the uncertainty of the total heat capacity is found to be lower than 10%. The total uncertainty in the ARB calculation is therefore considered to be lower than 20%.

#### Heat in Place (HIP)

Contrary to ARB, HIP is reservoir specific and gives the stored heat in the reservoir. The determination of HIP is based on exploration, confirming that the resources is technically exploitable. HIP is found to some extent in the previously described fairly permeable formations.

The basis for calculations is improved according to the explorations compared with the basis for determination of ARB. Uncertainty in the HIP determination therefore is considered to be less, probably around 10-15%.

#### Identified Resources (IR)

IR represents that part of the geothermal resource being economically and legally produceable as district heat energy. The temperature conversion between the geothermal and district heating water takes place by means of a heat pump plant. The detailed description of the method appears in Michelsen et al. 1980.

From experience, the economic drilling depth is about 3 km, the minimum mean reservoir temperature about 40 degrees C, and the minimum transmissivity about 5-10 Darcymetres, (see Koppe et al. 1983). These limits though may change in the future.

It is not considered, whether or not there are consumers of the produced heat within an economically acceptable distance from the geothermal heating plant.

Determining IR, the geothermal heating plants are assumed to be single doublet systems (i.e. one extraction and one injection well). If another design is chosen, IR as mentioned below can be changed essentially.

According to the uncertainties in the determination of HIP and RHW MAX, the uncertainty in the determination of IR is considered to be approximately 35-40%.

#### Max. Recovery Factor (RHW MAX)

The magnitude of RHW MAX is dependable on design and operation of the geothermal heating plant. For instance Gringarten (1978) shows, that production with reinjection of heat depleted water will increase the heat recovery by several orders of magnitude. Further greater lifetime and heat recovery factors are obtained by alternating injection and production wells. This is illustrated in Michelsen et al. 1980. For four Danish geothermal reservoirs it is shown, that, depending on the number and placing of extraction and injection wells, RHW MAX might vary within a range from 0 to 75%. Assuming an ideal well configuration a single doublet, a two doublet and a (theoretical) infinite lattice of doublets was found to have 25%, 40% and 75% max. recovery factors. The calculations are made as given by Gringarten (1978).

It is assumed that the geothermal resources are exploited in single doublet plants. The detailed description of the method appears in Michelsen et al. (1980).

RHW MAX is calculated as:

$$(7) \text{ RHW MAX} = \frac{S_c}{S_d} \times \frac{\bar{T} - T_i}{\bar{T} - T_o}$$

where  $S_c$  is theoretical area cooled by a single doublet exploitation.

$S_d$  is the area influenced by a geothermal doublet.

$\bar{T}$  is the mean reservoir temperature.

$T_i$  is the injection temperature of the heat depleted water.

$T_o$  is the mean annual temperature.

In France practical experience has shown, that the area ratio is about 0.33, see Lagivne (1978). The mean annual ground temperature in Denmark is about 8 degrees C, while the injection temperature is assumed to be 25 degrees C. Using these values in (7), (5) is found. The uncertainty on RHW MAX is considered to be up to 25%.

#### Identified Reserves (IRSVE)

In this report it has only been possible to estimate the Identified geothermal Reserves in Denmark roughly as 50% of the Identified Resources. However, because of uncertainty in most of the significant parameters and lack of practical experience in geothermal energy exploitation in Denmark there will always be great uncertainty about such an estimate. The uncertainty on the reserve determination is with the used method considered to be about 50%.

Still all identified reserves in Denmark is to be characterized as possible reserves grading towards the classification probable. However, soon the first practical experiences with geothermal heat exploitation will be made. During the last 3 years exploration and establishment of a single doublet pilot plant has been going on in Thisted and since the summer 1984 the plant has been in operation. Reference is made to Magtensgaard (1983).



## Results (Table 6-10 and figs. 13-17)

### Accessible Resource Base

For at typical, geological profile in the Danish Subbasin the accessible resources base is found to be

$$1450 \times 10^3 \text{ TJ/km}^2$$

(see Appendix II). This corresponds with the energy content in about 35 million tons of oil or the double of the yearly energy consumption in Denmark.

The calculated order of magnitude can be considered for the entire Danish area, and the total accessible, geothermal resource is estimated to about

$$60 \times 10^9 \text{ TJ.}$$

However, only a small ratio of this energy, the part stored in porous, geothermal reservoirs, can be exploited at the present time (compare with IR and IRSVE found below).

### Resources and Reserves

Heat in Place (HIP), Identified Resources (IR) and Identified possible Reserves (IRSVE) are determined for the porous geothermal reservoirs in the Bunter Sandstone, the Skagerrak, and the Gassum Formations and in the Haldager Sand and the Frederikshavn Member. The results and parameters making the basis for the determination are shown in table 6-10 and figs. 13-17. The following should be noticed:

The total value of HIP, IR and IRSVE in Denmark is calculated to

$770.1 \times 10^6$  TJ,  $206.4 \times 10^6$  TJ, and  $103.2 \times 10^6$  TJ respectively.

(See Appendix II).

Only about 25% (IR) of the geothermal heat stored in the reservoirs (HIP) can be exploited with the used method. Because of the cost of design and operation of the heat plant the gain in energy (IRSVE) is only about 13% of the stored heat.

The distribution of the total resources and reserves is about 3% in the Bunter Sandstone Formation, 70% in the Skagerrak Formation, 20% in the Gassum Formation, 3% in the Haldager Sand and 4% in the Frederikshavn Member.

If the economical minimum limits for mean reservoir temperature (40 degrees C) and transmissivity (10 Darcymetres) given by Koppe et. al. (1983) is considered, the results for HIP, IR and IRSVE has to be reduced with 35%. Practically all geothermal energy stored in the Bunter Sandstone, Haldager Sand, Frederikshavn Member, and more than 80% of the energy stored in the Gassum Formation has to be left out of consideration. However, it is not known whether the limits given by Koppe is valid for geothermal heat exploitation (with the actual method) in Denmark. Further these limits might change in the future.

### Conclusion and postscript

It has been shown, that geothermal reservoirs of interest are present in Denmark. The reservoirs are analysed in the depth intervals between 500 m and 3000 m below ground level. The geothermal heat stored in the reservoirs is determined to be

$$7.7 \times 10^8 \text{ TJ.}$$

Assuming an exploitation with single doublets and heat pump plants, the possible gain in energy is about

$$1.0 \times 10^8 \text{ TJ.}$$

To throw this in relief the total heat demand in Denmark is about

$$1.66 \times 10^5 \text{ TJ.}$$

per year (see Appendix III). The demand distribution is illustrated in fig. 19.

Comparing the heat demand distribution in fig. 19 with the determined possible geothermal reserves in tables 6-10 and figs. 13-17 it immediately seems possible to supply most of the heat demand in Denmark from geothermal heat plants. To exploit the geothermal resources in a certain area economically it is still a condition, that a relatively high and concentrated heat demand (e.g. a high district heating demand) is present nearby the plant, see Michelsen (1980). As shown in Dansk Olie & Naturgas A/S et. al (1980) & (1982) only a number of such areas can be found in Denmark, situated outside larger cities, where coproduction of electricity and district heating takes place. Therefore it is only realistic, that a smaller

part of the heat demand can be supplied from geothermal heat plants, although the possible reserves can supply the yearly demand several times.

The results presented in this report have been based on data and conclusions from wells drilled up to the year 1983. Since then further reservoir studies have been carried out as well as new wells have been drilled to test the Haldager and Gassum Formation (Thisted) and the Bunter Sandstone (Tønder).

In both areas the reservoirs are at depths above 2000 metres. The reservoir rocks are unconsolidated to slightly consolidated sands, which have proven to have marked better reservoir properties than encountered and predicted up to then in more consolidated and deeper reservoirs. This new approach of drilling reservoirs in the depth range of 500-1500 metres may prove very rewarding for future geothermal exploration.

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## Appendix I. Uncertainty about total heat capacity

The total heat capacity in a reservoir is determined as:

$$C_t = \emptyset \times C_w + (1 - \emptyset) \times C_r$$

where  $\emptyset$  is the reservoir porosity

$C_w$  is the heat capacity of the fluid (per unit volume)

$C_r$  is the heat capacity of the rock (per unit volume)

The uncertainty about  $C_t$  depends on the three significant parameters:

### Heat capacity of the fluid ( $C_w$ )

$C_w$  depends on temperature and salinity. The temperature depth relation is simplified as:

$$T = 10 + 0.030 \times d \quad (^\circ\text{C})$$

where  $T$  = is the temperature ( $^\circ\text{C}$ )

$d$  is depth (m)

The salinity is estimated to 10‰ at 1000 m, 18‰ at 2000 m, and 26‰ beyond 3000 m. From these relations  $C_w$  is determined in table I. 1. The uncertainty about  $C_w$  introduced by the simplified temperature and salinity relations is assessed to be less than +/- 5%.



Table I.1. Calculations of  $C_W$  based on simplified depth relations of temperature and salinity.

---

Depth m	Temp. °C	Salinity %wt.	C.avg.heat Kj/kg°C*)	P, density Kg/m <sup>3</sup> *)	$C_W$ Mj/m <sup>3</sup> °C
1000	40	10	3.70	1060	3.92
2000	70	18	3.41	1035	3.70
3000	100	26	3.23	1120	3.62
4000	130	26	3.23	1105	3.57
5000	160	26	3.25	1090	3.54

\*) Values from L. Berkeley Lab.: Aqueous Sol. Database to High. Temp. and Press. NaCl Solutions.

Heat capacity of the rock ( $C_r$ )

$C_r$  is about 2.2 MJ/(m<sup>3</sup> x C). The uncertainty about this value is +/- 5%.

Porosity ( $\emptyset$ )

The variation in  $\emptyset$  is given in table I.2 at different depths to the Skagerrak and Gassum Formations and the Haldager Sand.  $C_t$  is calculated from the above given values of  $C_W$  and  $C_r$  and the porosities given in table I.2. This gives the distribution shown in fig. 18. It is seen that for all formations the variations in  $C_t$  is less than +/- 5%.

Total uncertainty about  $C_t$

From the evaluations shown above the total uncertainty about  $C_t$  is estimated to be less than 10%.

Table I.2. Porosity variations of the Skagerrak Formation, Gassum Formation and Haldager Sand.

Skagerrak Formation

depth m b.MSL	porosity		
	avr.	min.	max.
2000	20	15	25
3000	15	10	20
4000	9	5	13
5000	5	2	8

Gassum Formation

1000	30	23	40
2000	21	14	28
3000	12	9	16

Haldager Sand

1000	30	23	37
2000	22	16	27

## Appendix II. Calculation of ARB

The accessible resource base (ARB) is found by integration as:

$$(1) \text{ ARB} = \int_0^h C_t(h) \times (T(h=0)) \times dh$$

where  $C_t(h)$  is the total heat capacity at depth  $h$

$T(h)$  is the temperature at depth  $h$

$h$  is the depth below ground level

The ARB calculation is based on the knowledge about the stratigraphic profile in the Danish Subbasin. This is illustrated in table II.1., where the units are characterized by lithology, porosity and vertical extension of the layers. The profile during the calculation is separated in (N) intervals, where  $C_t$  is approximately constant. (1) then can be rewritten to

$$(2) \text{ ARB} = \sum_{i=1}^N \int_{h_{i-1}}^{h_i} C_{ti} (T(h) - T(h=0)) dh$$

According to table II.1. the intervals are separated at the following depths:

100, 1750, 2400, 2450, 3150, 3300, 4400, 6500 and 7000 metres below ground level.

The rise in temperature is assumed constant  $0.028^\circ\text{C}/\text{m}$  from the ground level through the first five layers (0-3150). Below this is assumed a temperature rise of  $0.020^\circ\text{C}/\text{m}$ .

$$(3) T(h) = T(h=0) + 0.028 \times h; \quad 0 \leq h \leq 3150 \text{ m}$$

$$T(h) = T(h=3150) + 0.020 \times (h-3150); \quad 3150 \text{ m} \leq h \leq 7000 \text{ m}$$

(2) and (3) gives:

$$(4) \text{ ARB} = \sum_{i=1}^5 \int_{h_{i-1}}^{h_i} \{ C_{ti} (0.028 \times h) dh \} + \sum_{i=6}^9 \int_{h_{i-1}}^{h_i} \{ C_{ti} (T(3150) - T(o) + 0.020(h-3150)) dh \}$$

which integrated gives:

$$(5) \text{ ARB} = \frac{1}{2} \times 0.028 \sum_{i=1}^5 \{ C_{ti} (h_i^2 - h_{i-1}^2) \} + 0.020 \sum_{i=6}^9 \{ C_{ti} (\frac{1}{2} h_i^2 - 3150 h_i + \frac{1}{2} h_{i-1}^2 + 3150 h_{i-1}) \} + (T(3150) - T(o)) \sum_{i=6}^9 \{ C_{ti} (h_i - h_{i-1}) \}$$

As the heat capacity of sandstone is used 2.2 MJ/(m<sup>3</sup> x °C). In lack of better information the same value is used for clay- and limestone, while the heat capacity of rock salt is about 2.0 MJ/(m<sup>3</sup> x °C). The variation in fluid heat capacity is calculated as shown in APP.I (the same variation in salinity is used). The calculation of total heat capacity is shown in table II.2.

In table II.2. the calculation of ARB is shown. The total accessible resource base is estimated to 1.45 x 10<sup>6</sup> TJ/km<sup>2</sup>. It is worth noticing, that only about 25% of ARB is found above a depth of 3150 m.

Table II.1. Simplified stratigraphic column  
of the Danish Subbasin

Period	m b.MSL	Lithology	Porosity %		
			avg.	min	max
Quarternary	0-100	claystone	49	42	55
U.Cretaceous	100-1750	limestone	23	10	29
-	100-350	-	28	26	29
-	350-650	-	25	22	28
-	650-800	-	27	25	28
-	800-1000	-	23	20	27
-	1000-1100	-	20	15	25
-	1100-1750	-	14	10	18
L.Cretaceous	1750-2150	claystone	30	28	32
U.Jurassic	2150-2350	-	20	18	25
-	2350-2400	-	27	24	30
M.Jurassic	2400-2450	sandstone	22	20	27
L.Jurassic	2450-3150	claystone	18	15	21
L.Jurassic/ U.Triassic	3150-3300	sandstone	12	9	17
Triassic	3300-4400	claystone/salt	15	12	18
-	4400-6500	sandstone/clayst.	5	0	10
Zechstein	6500-7000	salt	0	-	-

Interval	Depth	Temp.	Salinity	Fluid heat capacity	Rock heat capacity	Porosity	Total heat capacity	Acc.Resource Base
i	h m	$\bar{T}$ °C	%wt	$C_w$ MJ/(m <sup>3</sup> x °C)	$C_r$ MJ/(m <sup>3</sup> x °C)	$\emptyset$ %	$C_t$ MJ/(m <sup>3</sup> x °C)	ARB 10 <sup>9</sup> MJ/km <sup>3</sup>
1	0-100	9	0	4.19	2.2	49	3.2	0.4
2	100-1750	34	9	3.95	2.2	23	2.6	111.1
3	1750-2400	66	18	3.71	2.2	25	2.6	98.2
4	2400-2450	76	22	3.68	2.2	22	2.5	8.5
5	2450-3150	86	24	3.66	2.2	18	2.5	137.2
6	3150-3300	98	26	3.63	2.2	12	2.4	32.2
7	3300-4400	110	26	3.61	$\frac{2.2+2.0}{2}$	15	2.3	258.1
8	4400-6500	142	26	3.56	2.2	5	2.3	647.2
9	6500-7000	168	26	3.54	2.0	0	2.0	160.0
							Total ARB:	1452.9

Assumptions:  $T(o) = 8^\circ\text{C}$

Table II.2. Calculation of Accessible Resource Base

Appendix III. Netto heat demand

The netto heat demand of Denmark is tabulated in table III.1 and illustrated on fig. 19.

The data are based on a preliminary summary prepared by The Danish Energy Agency, 1983. The data are collected by DEA from the counties and other local authorities.

Table III.1 Netto heat demand according to counties and heating type, TJ/year, status.

County	District	Block heating	Gas heat- ing	Central heat- ing	Electri- cal heating	Unspe- cified	Total
Metro- politan area	10761	2511	1358	17413	562	5987	38591
Frederiks- borg	1345	371	78	6628	1015	902	10339
Roskilde	828	64	4	3901	569	283	5648
West- sjælland	1430	488	66	6628	756	2101	11469
Storstrøm	1256	52	1	6004	654	1057	9024
Bornholm	-	-	-	-	-	-	1500
Fyn	6324	124	32	8794	221	584	15478
South- jylland	2286	547	3	5741	500	476	9552
Ribe	3640	115	0	3534	188	198	7675
Vejle	3334	249	6	7632	259	424	11904
Ring- købing	3389	45	-	4400	129	278	8241
Århus	6162	44	-	6993	245	122	13568
Viborg	1670	13	2	3741	113	381	5919
North- jylland	6761	381	20	8497	330	710	16699
Total							165607

Basic data tabulation

Table 1

BUNTER SANDSTONE FORMATION

Region	S. Jylland	Loll.-Falster	S. Sjælland	Fyn	
Depth interval, km	1.4-2.1	1.0-1.5	1.5-2.0	1.0-1.5	
Temp. % mean depth	60	48	58	45	
Porosity % mean	28	27	25	30	
<hr/>					
Brine- permeab. mD	average	250	200	100	400
	max.	1100	1100	400	800
	min.	30	35	35	100
<hr/>					
Netresou. thickness m	average	35	30	50	5
	max.	60	50	75	15
	min.	5	20	20	0
<hr/>					
Transmiss. Dm	average	9	6	5	2
	max.	15	10	7.5	7.5
	min.	1.5	0.5	2	0
<hr/>					
Area km <sup>2</sup>	2500	2300	2000	2500	
<hr/>					



Basic data tabulation

Table

SKAGERRAK FORMATION

Region	Vendsyssel	Vendsyssel	Vendsyssel	Himmerland	Thy-Himmerl.	Thy
Depth interval, km	0.5-1.0	1.0-1.5	1.5-2.0	1.5-2.0	2.5-3.0	1.0-1.5
Temp. % mean depth	40	55	65	75	93	50
Porosity % mean	26	24	24	24	16	24
Brine-permeab. mD	average	250	180	180	45	280
	max.		1000	1000	100	
	min.				10	
Netresou. thickness m	average	40	50	50	200	270
	max.	55				
	min.	25				
Transmis. Dm	average	10	10	10	9	75
	max.	14			20	
	min.	6			2	
Area km <sup>2</sup>	500	1090	200	100	2000	320
Region	Central	Jylland	NW Jylland			
Depth interval, km	2.0-2.5	2.5-3.0	>3			
Temp. % mean depth	71	85	115			
Porosity % mean	18	16	12			
Brine-permeab. mD	average	120	45	8		
	max.		100	45		
	min.		10	3		
Netresou. thickness m	average	100	250	500		
	max.		450	1000		
	min.		100			
Transmis. Dm	average	12	11	4		
	max.		20	8		
	min.		5			
Area km <sup>2</sup>	3000	3500	3500			
Region	S.-M. Sjælland	M.-N. Sjælland	N.-M. Sjælland	Sjælland	Sjælland	
Depth interval, km	1.5-2.0	2.0-2.5	2.0-2.5	2.5-3.0		
Temp. % mean depth	63	70	75	88		
Porosity % mean	21	18	18	16		
Brine-permeab. mD	average	200	120	120	45	
	max.				100	
	min.				10	
Netresou. thickness m	average	50	200	250	250	
	max.	75		450		
	min.	20		100		
Transmis. Dm	average	10	24	30	11	
	max.	15		50		
	min.	4		10		
Area km <sup>2</sup>	1950	2800	550	1250		

Basic data tabulation

GASSUM FORMATION

Table 3

Region	Vendsyssæl	Vendsyssæl	Vendsyssæl	Vendsyssæl	Himml.-Thy	
Depth interval, km	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	2.5-3.0	
Temp. % mean depth	40	55	70	80	95	
Porosity % mean	33	30	24	19	15	
Brine-permeab. mD						
average	200	350	300	50	35	
max.	400	1400		70		
min.	100	100		5		
Netresou. thickness m						
average	15	50	50	60	60	
max.	25	75	75	90	90	
min.	5	25	25	30	30	
Transmis. Dm						
average	3	18	15	3	2	
max.	10	40	23	4.5	3.5	
min.	1	3	8	1.5	1	
Area km <sup>2</sup>	850	910	660	1110	1100	
Region	E.Middle Jyll.	E.Jylland	Central	Jylland	Central	Jylland
Depth interval, km	1.0-1.5	1.5-2.0	2.5-3.0	>3	1.5-2.0	2.0-2.5
Temp. % mean depth	50	65	85	110	60	75
Porosity % mean	28	24	15	<13	24	19
Brine-permeab. mD						
average	200	300	35	8	80	20
max.	1400	450			450	100
min.	45	15			15	5
Netresou. thickness m						
average	25	50	50	80	20	25
max.	50	75	70	110	30	70
min.	10	25	30	50	10	15
Transmis. Dm						
average	5	15	1.5	0.6	2	0.5
max.	25	22	3		3	1.5
min.	1	7.5	0.5		1	0.3
Area km <sup>2</sup>	900	890	2000	1100	2910	4380
Region	S.Denmark	M.-S.Sjælland	Sjælland		Fyn	
Depth interval, km	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	1.0-1.5	
Temp. % mean depth	35	50	60	70	47	
Porosity % mean	33	28	24	19	28	
Brine-permeab. mD						
average	1000	200	150	100	200	
max.	1400	1400	450	200	1400	
min.	100	45	15	10	45	
Netresou. thickness m						
average	50	70	90	80	60	
max.	75	100	130	100	90	
min.	10	40	50	60	30	
Transmis. Dm						
average	50	14	12	8	12	
max.	75	50	25	10	45	
min.	2	2	6	6	2	
Area km <sup>2</sup>	500	1950	2810	1340	320	

Basic data tabulation

HALDAGER SAND

Table

Region	Vendsyssel		East Jylland	NW Jylland	NW Jylland	NW Jylland
Depth interval, km	0.5-1.0	1.0-1.5	1.0-1.5	1.5-2.0	2.0-2.5	>3
Temp. % mean depth	35	45	55	65	75	95
Porosity % mean	31	28	28	24	20	15
<hr/>						
Brine-permeab.	$D_p$ average	2000	800	800	200	90
	$D_p$ max.	7500	3000			180
	$D_p$ min.	350	200			
<hr/>						
Netresou. thickness	$D_m$ average	15	45	5	10	20
	$D_m$ max.	40	90		20	45
	$D_m$ min.	5	10		5	5
<hr/>						
Transmiss.	$D_m$ average	30	36	4	2	9
	$D_m$ max.	80	135		10	15
	$D_m$ min.	10	9			
<hr/>						
Area km <sup>2</sup>	1450	1730	770	3430	3000	500

Region	Himmerland	Central N.Jylland
Depth interval, km	2.5-3.0	2.5-3.0
Temp. % mean depth	85	75
Porosity % mean	16	16

Brine-permeab.	$D_p$ average	20	20
	$D_p$ max.	90	
	$D_p$ min.		
<hr/>			
Netresou. thickness	$D_m$ average	25	10
	$D_m$ max.	40	
	$D_m$ min.	10	
<hr/>			
Transmiss.	$D_m$ average	0.5	0.2
	$D_m$ max.	3.5	
	$D_m$ min.		
<hr/>			
Area km <sup>2</sup>	300	650	

Bacis data tabulation

FREDERIKSHAVN MEMBER

Table 5

Region	S. Vendsyssel						
	N.Vendsyssel	Himmerland	NW Jylland	NW Jylland	NW Jylland	NW Jylland	
Depth interval, km	0.5-1.0	0.5-1.0	0.1-1.5	1.5-2.0	2.0-2.5	2.5-3.0	
Temp. % mean depth	27	32	45	55	70	70	
Porosity % mean	32	32	27	23	18	13	
<hr/>							
Brine- permeab. mD	average	250	250	150	100	40	20
	max.						
	min.						
<hr/>							
Netresou. thickness m	average	70	20	30	20	15	20
	max.	100	30	40	40	20	
	min.	40	10	10	0	0	
<hr/>							
Transmiss. Dm	average	18	5	4.5	2	0.6	0.4
	max.	25	7.5	6	4	1	
	min.	10	2.5	1	0	0	
<hr/>							
Area km <sup>2</sup>	2380	1590	7600	7000	1170	360	

**Resource and Reserve Calculations**  
**BUNTER SANDSTONE FORMATION**

Table 6

Region		S. Jylland	Lolland- Falster	S. Sjælland	Fyn	Total
Depth b. MSL	(m)	1.4-2.1	1.0-1.5	1.5-2.0	1.0-1.5	
Mean temperature	(°C)	60	48	58	45	
Porosity	(%)	28	27	25	30	
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C )		2.50	2.50	2.45	2.55	
Res. thickness	(m)	35	30	50	5	
Transmissivity	(Dm)	9*	6*	5*	2*	
Area	(km <sup>2</sup> )	2500	2300	2000	2500	
Heat in Place	(10 <sup>6</sup> TJ)	11.4	6.9	12.3	1.2	31.8
Max. Recov. Fact.	(-)	0.22	0.19	0.22	0.18	
Ident. Resources (10 <sup>6</sup> TJ)		2.5	1.3	2.7	0.2	6.7
Possible Reserves (10 <sup>6</sup> TJ)		1.3	0.6	1.4	0.1	3.4
	(TJ/km <sup>2</sup> )	520.0	260.7	700.0	40.0	

Please refer to the text for the derivation and uncertainty of the above mentioned values.

\* Values below 40° C or 10 Dm, the limit for economical plants given by Koppe et. al. (1983).

**Resources and Reserves Calculations**  
**SKAGERRAK FORMATION**

Table 7

Region		Vendsyssel	Vendsyssel	Vendsyssel	Himmerland	Thy-Himml.	Thy	Central Jylland	Central Jylland
Depth b. MSL	(m)	0.5-1.9	1.0-1.5	1.5-2.0	1.5-2.0	2.5-3.0	1.0-1.5	2.0-2.5	2.5-3.0
Mean temperature	(°C)	40	55	65	75	93	50	71	85
Porosity	(%)	26	24	24	24	16	24	18	16
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C)		2.65	2.60	2.57	2.54	2.43	2.60	2.47	2.43
Res. thickness	(m)	40	50	50	50	200	270	100	250
Transmissivity	(Dm)	10	10	10	10	9*	75	12	11
Area	(km <sup>2</sup> )	500	1090	200	100	2000	320	3000	3500
Heat in Place	(10 <sup>6</sup> TJ)	1.7	6.7	1.5	0.9	82.6	9.4	46.7	163
Max. Recov. Fact.	(-)	0.15	0.21	0.23	0.25	0.26	0.20	0.24	0.26
Ident. Resources	(10 <sup>6</sup> TJ)	0.3	1.4	0.3	0.2	21.5	1.9	11.2	42.6
Possible Reserves	(10 <sup>6</sup> TJ)	0.2	0.7	0.2	0.1	10.7	1.0	5.6	21.3
	TJ/km <sup>2</sup>	400.0	642.2	1000.0	1000.0	5350.0	3125.0	1866.7	6085.7

Region		S.-M. Sjælland	M.-N. Sjælland	N.-M. Sjælland	Sjælland	Total
Depth b. MSL	(m)	1.5-2.0	2.0-2.5	2.0-2.5	2.5-3.0	
Mean temperature	(°C)	63	70	75	88	
Porosity	(%)	21	18	18	16	
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C)		2.53	2.47	2.46	2.43	
Res. thickness	(m)	50	200	250	250	
Transmissivity	(Dm)	10	24	30	11	
Area	(km <sup>2</sup> )	1950	2800	550	1250	
Heat in Place	(10 <sup>6</sup> TJ)	13.6	85.6	22.7	60.8	495.9
Max. Recov. Fact.	(-)	0.23	0.24	0.25	0.26	
Ident. Resources	(10 <sup>6</sup> TJ)	3.1	42.8	5.7	15.8	146.8
Possible Reserves	(10 <sup>6</sup> TJ)	1.5	21.4	2.8	7.9	73.4
	TJ/km <sup>2</sup>	769.2	7642.9	5090.9	6320.0	

Please refer to the text for the derivation and uncertainty of the above mentioned values.

\* Values below 40° C or 10 Dm, the limit for economical plants given by Koppe et.al. (1983).

## Resources and Reserve Calculations

Table 8

Region	GASSUM FORMATION									
	Vendsyssel	Vendsyssel	Vendsyssel	Vendsyssel- Himmerland	Himmerland- Thy	E.-M. Jylland	E.- Jylland			
Depth b. MSL	(m)	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	2.5-3.0	1.0-1.5	1.5-2.0		
Mean temperature	(°C)	40	55	70	80	95	50	65		
Porosity	(%)	33	30	24	19	15	28	24		
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C)		2.78	2.68	2.56	2.48	2.41	2.66	2.57		
Res. thickness	(m)	15	50	50	60	60	25	50		
Transmissivity	(Dm)	3*	18	15	3*	2*	5*	15		
Area	(km <sup>2</sup> )	850	910	660	1110	1110	900	890		
Heat in Place	(10 <sup>6</sup> TJ)	1.1	5.7	5.2	11.9	14.0	2.5	6.5		
Max. Recov. Fact.	(-)	0.15	0.21	0.24	0.25	0.27	0.20	0.23		
Ident. Resources	(10 <sup>6</sup> TJ)	0.2	1.2	1.3	3.0	3.8	0.5	1.5		
Possible Reserves	(10 <sup>6</sup> TJ)	0.1	0.6	0.7	1.5	1.4	0.3	0.7		
	(TJ/km <sup>2</sup> )	117.6	659.3	1060.6	1351.4	1261.3	333.3	786.5		
Region		Central Jylland	Central Jylland	Central Jylland	Fyn	S.- Denmark	M.-S.- Sjælland	Sjælland	Sjælland	Tota
Depth b. MSL	(m)	1.5-2.0	2.0-2.5	2.5-3.0	1.0-1.5	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	
Mean temperature	(°C)	60	75	85	47	35*	50	60	70	
Porosity	(%)	24	19	15	28	33	28	24	19	
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C)		2.57	2.48	2.42	2.66	2.80	2.66	2.57	2.48	
Res. thickness	(m)	20	25	50	60	50	70	90	80	
Transmissivity	(Dm)	2*	0.5*	1.5*	12	50	14	9*	8*	
Area	(km <sup>2</sup> )	2910	4380	2000	320	500	1950	2810	1340	
Heat in Place	(10 <sup>6</sup> TJ)	7.8	18.2	18.6	2.0	1.9	15.2	33.8	16.5	160.
Max. Recov. Fact.	(-)	0.22	0.25	0.26	0.19	0.12	0.20	0.22	0.24	
Ident. Resources	(10 <sup>6</sup> TJ)	1.7	4.5	4.8	0.4	0.2	3.0	7.4	4.0	37.
Possible Reserves	(10 <sup>6</sup> TJ)	0.9	2.3	2.4	0.2	0.1	1.5	3.7	2.0	18.
	(TJ/km <sup>2</sup> )	309.3	525.1	1200.0	625.0	200.0	769.2	1316.7	1492.5	

Please refer to the text for the derivation and uncertainty of the above mentioned values.

\* Values below 40° C or 10 Dm, the limit for economical plants given by Koppe et.al. (1983)

## Resources and Reserve Calculation

Table 9

Region	Vendsyssel	Vendsyssel	HALDAGER SAND		Himmerland	Central N.Jylland	E.-Jylland	Total
			N.-W. Jylland	N.-W. Jylland				
Depth b. MSL (m)	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	2.5-3.0	2.5-3.0	1.0-1.5	
Mean temperature (°C)	35*	45	65	75	85	75	55	
Porosity (%)	31	28	24	20	16	16	28	
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C)	2.76	2.67	2.57	2.50	2.43	2.44	2.66	
Res. thickness (m)	15	45	10	20	25	10	5	
Transmissivity (Dm)	30	36	2*	9*	0.5*	0.2*	4*	
Area (km <sup>2</sup> )	1450	1730	3430	3000	300	650	770	
Heat in Place (10 <sup>6</sup> TJ)	1.6	7.7	5.0	10.1	1.4	1.1	0.5	27.4
Max. Recov. Fact. (-)	0.12	0.18	0.23	0.25	0.26	0.25	0.21	
Ident. Resources (10 <sup>6</sup> TJ)	0.2	1.4	1.2	2.5	0.4	0.3	0.1	6.1
Possible Reserves (10 <sup>6</sup> TJ)	0.1	0.7	0.6	1.2	0.2	0.2	0.1	3.1
(TJ/km <sup>2</sup> )	69.0	404.6	174.9	400.0	666.7	307.7	129.9	

## FREDERIKSHAVN MEMBER

Table 10

Region	N.-Vendsyssel	S.-Vendsys. Himmerland	N.W. Jylland	N.W. Jylland	N.W. Jylland	N.W. Jylland	Total
Mean temperature (°C)	27*	32*	45	55	70	70	
Porosity (%)	32	32	27	23	18	13	
Tot. Heat. Cap. (MJ/m <sup>3</sup> °C)	2.80	2.79	2.65	2.57	2.47	2.39	
Res. thickness (m)	70	20	30	20	15	20	
Transmissivity (Dm)	18	5*	4.5*	2.0*	0.6*	0.4*	
Area (km <sup>2</sup> )	2380	1590	7600	7000	1170	360	
Heat in Place (10 <sup>6</sup> TJ)	8.9	2.1	22.4	16.9	2.7	1.1	54.1
Max. Recov. Fact. (-)	0.03	0.10	0.18	0.21	0.24	0.24	
Ident. Resources (10 <sup>6</sup> TJ)	0.3	0.2	4.0	3.6	0.6	0.3	9.0
Possible Reserves (10 <sup>6</sup> TJ)	0.1	0.1	2.0	1.8	0.3	0.2	4.5
(TJ/km <sup>2</sup> )	42.0	62.9	263.2	257.1	256.4	555.6	

Please refer to the text for the derivation and uncertainty of the above mentioned values.

\* Values below 40° C or 10 Dm, the limit for economical plants given by Koppe et.al. (1983).





FIGURES



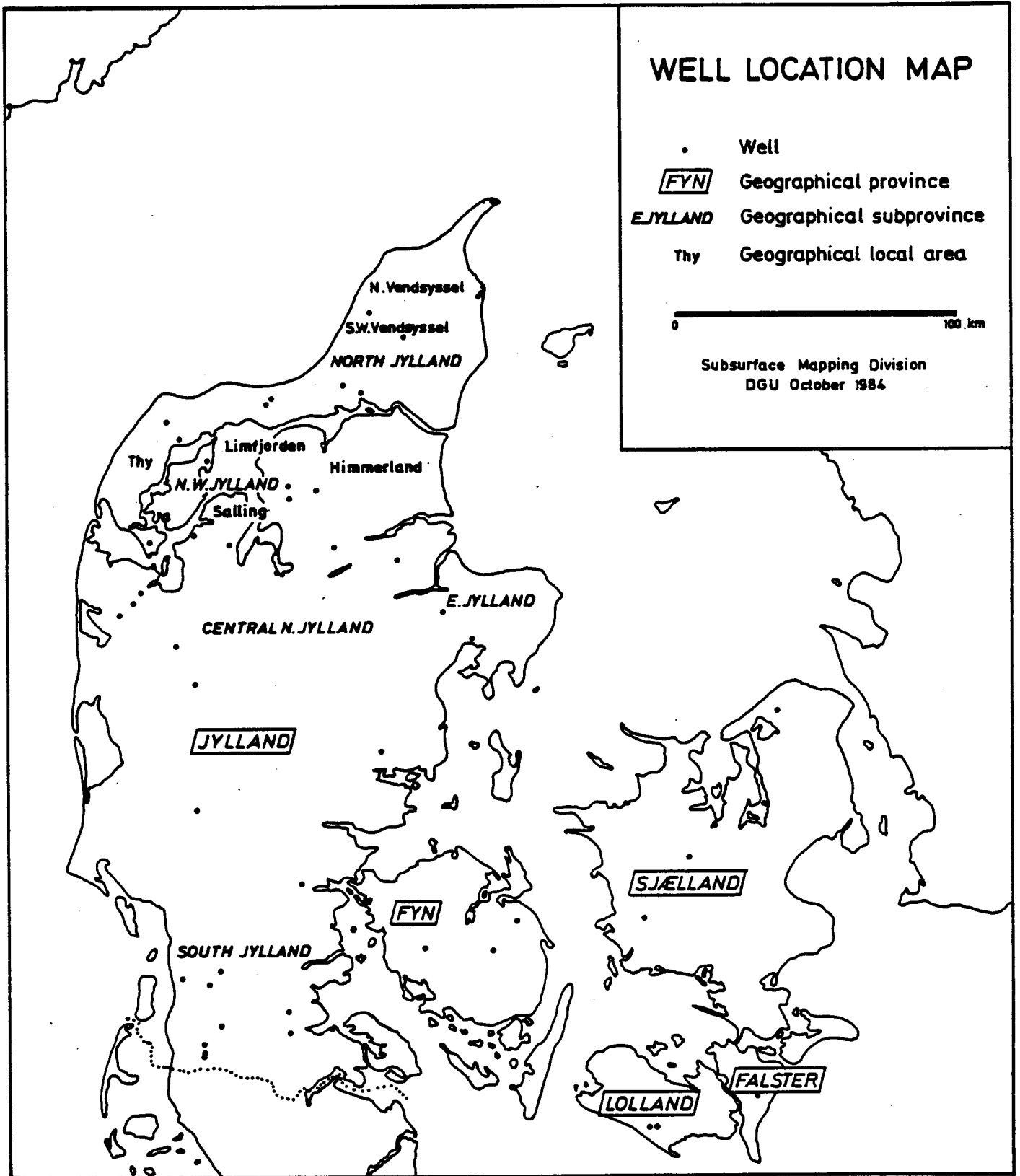


Fig.1

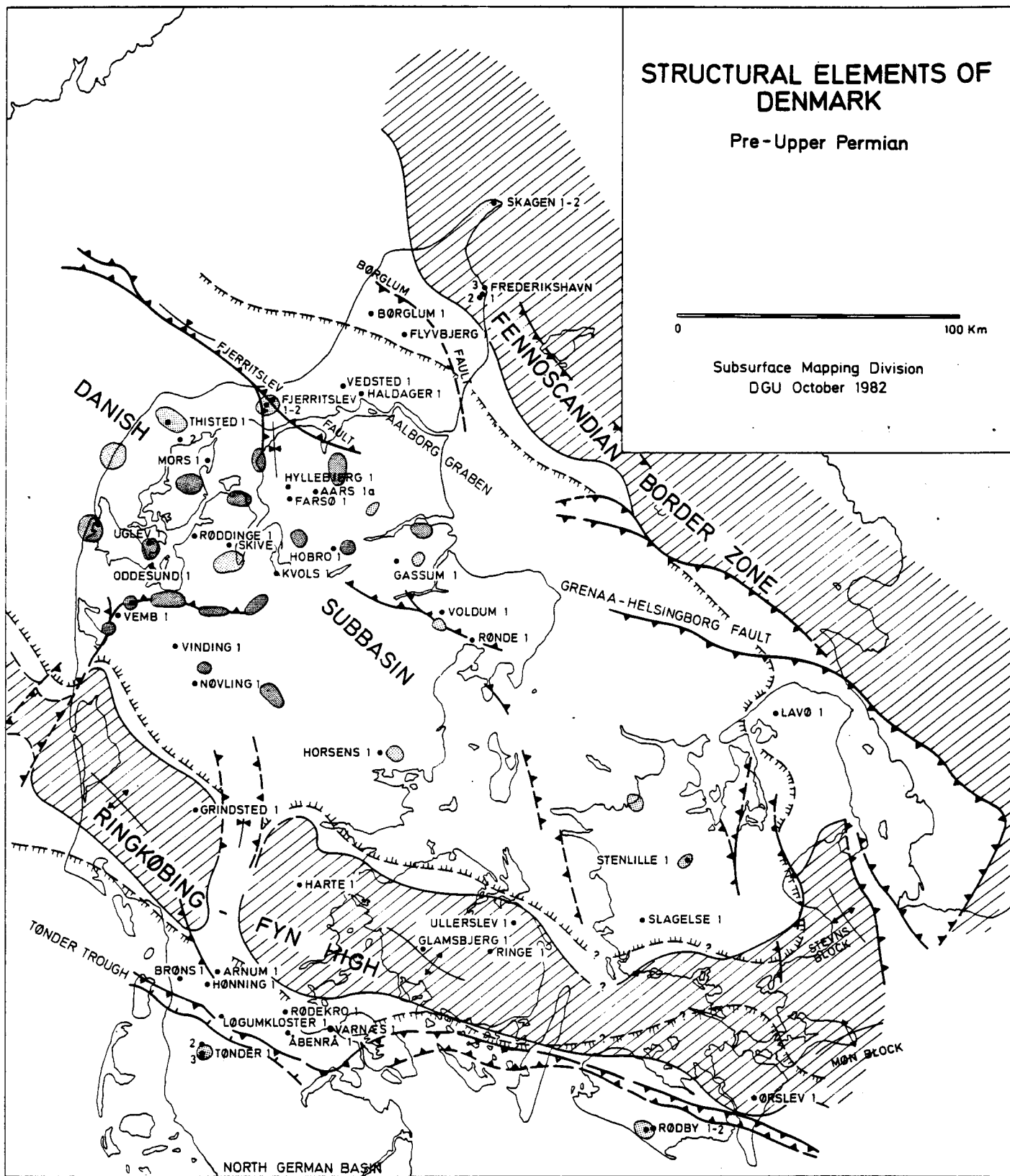


# STRUCTURAL ELEMENTS OF DENMARK

Pre-Upper Permian

0 100 Km

Subsurface Mapping Division  
DGU October 1982



Legend:

- |  |                         |  |                                 |
|--|-------------------------|--|---------------------------------|
|  | Major fault             |  | Extension of Zechstein deposits |
|  | Major fault (uncertain) |  | Positive areas                  |
|  | Low trend               |  | Salt pillow                     |
|  | High                    |  | Salt piercement                 |
|  |                         |  | Well site                       |

Fig.2



**STRATIGRAPHIC SUBDIVISION  
OF  
THE DANISH ONSHORE AREA**

SYSTEM	SERIES	STAGE	GROUP		FORMATION	MEMBER
TERTIARY and younger						
CRETACEOUS	UPPER		CHALK GROUP			
	LOWER	ALBIAN			RØDBY FORMATION	
		APTIAN BARREMIAN HAUTERIAN VALANGINIAN			VEDSTED FORMATION	
		BERRIASIAN				* FREDERIKSHAVN MEMBER C B A
JURASSIC	UPPER	PORTLANDIAN			BREAM FORMATION	ØRGLUM MEMBER
		KIMMERIDGIAN				
		OXFORDIAN				
	MIDDLE	CALLOVIAN BATHONIAN BAJOCIAN			HALDAGER FORMATION	FLYVBJERG MEMBER * HALDAGER SAND
		AALENIAN TOARCIAN				MEMBER F-IV MEMBER F-III
	LOWER	U. PLIENSBACHIAN			FJERRITSLEV FORMATION	MEMBER F-II c b a
		L. PLIENSBACHIAN				
		U. SINEMURIAN				
		L. SIN. - HETTANGIAN				MEMBER F-I b a
	TRIASSIC	UPPER	RHAETIAN	RHAETIC	MORS GROUP	GASSUM FORMATION
NORIAN					* VINDING FORMATION	
CARNIAN			KEUPER	JYLLAND GROUP	ODDESUND FORMATION	MEMBER O <sub>3</sub> MEMBER O <sub>2</sub> MEMBER O <sub>1</sub>
MIDDLE		LADINIAN			TØNDER FORMATION	
		ANISIAN	MUSCHEL-KALK	LOLLAND GROUP	FALSTER FORMATION	
LOWER		OLENIKIAN	Röt		ØRSLEV FORMATION	
		JAKUTIAN	BUNTSANDSTEIN	BACTON GROUP	BUNTER SAND-STONE FORMATION	*
		BRAMANIAN			BUNTER SHALE FORMATION	
					SKAGERRAK FORMATION	
PERMIAN and older						
					ZECHSTEIN	

\* RESERVOIR FORMATIONS DISCUSSED IN THIS REPORT

OGU 1984

Fig. 3



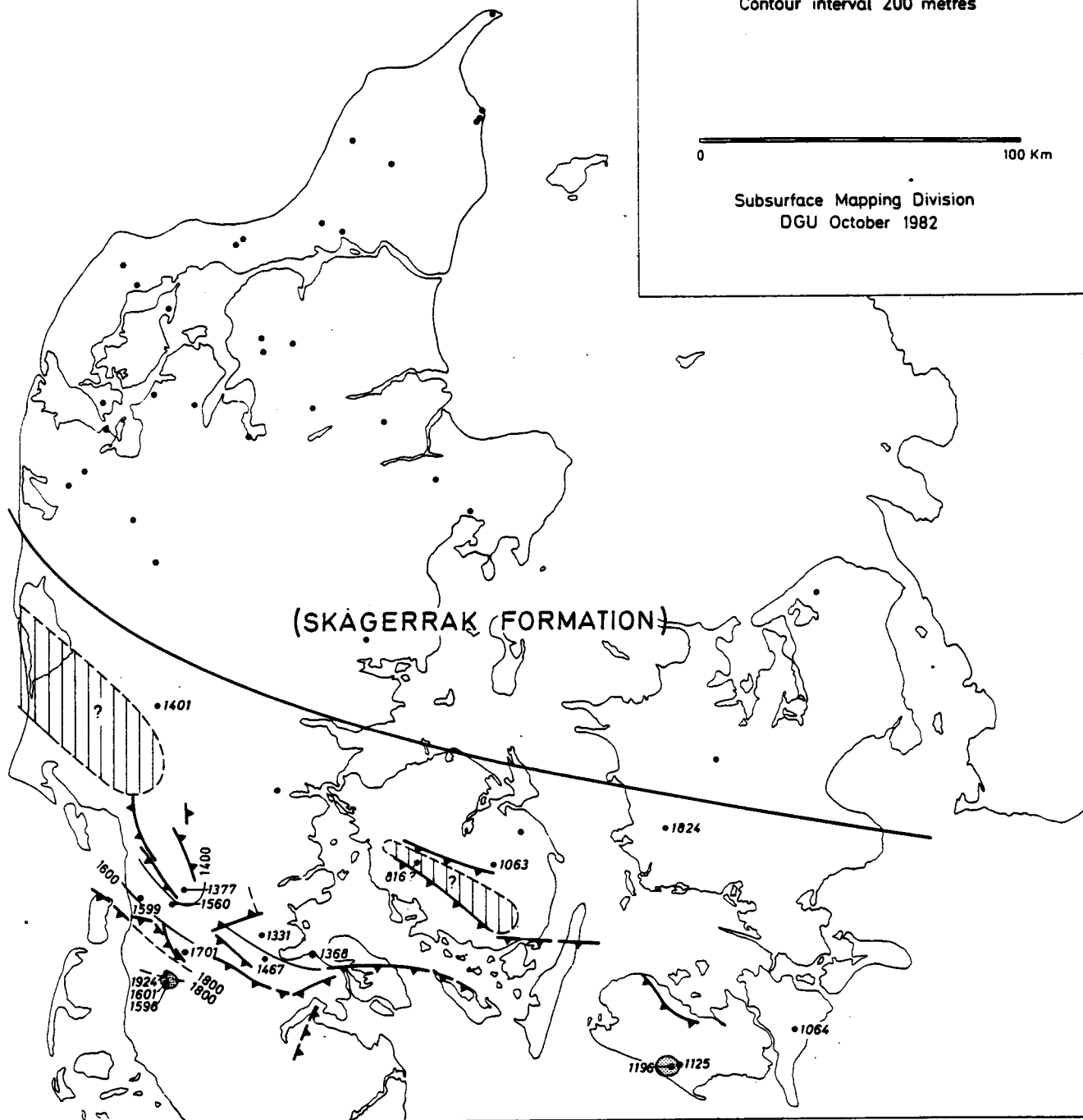


# TOP BUNTER SANDSTONE FORMATION

Generalized Depth Map  
Depth in metres below M.S.L.  
Contour interval 200 metres

0 100 Km

Subsurface Mapping Division  
DGU October 1982



Legend :

--- Fault (questionable)

— Fault (certain)

● Salt pillow

||||| Bunter Sandstone Formation thin or absent

— Depth contour

- - - Depth contour (uncertain)

• 1064 Depth from well data

Fig.4



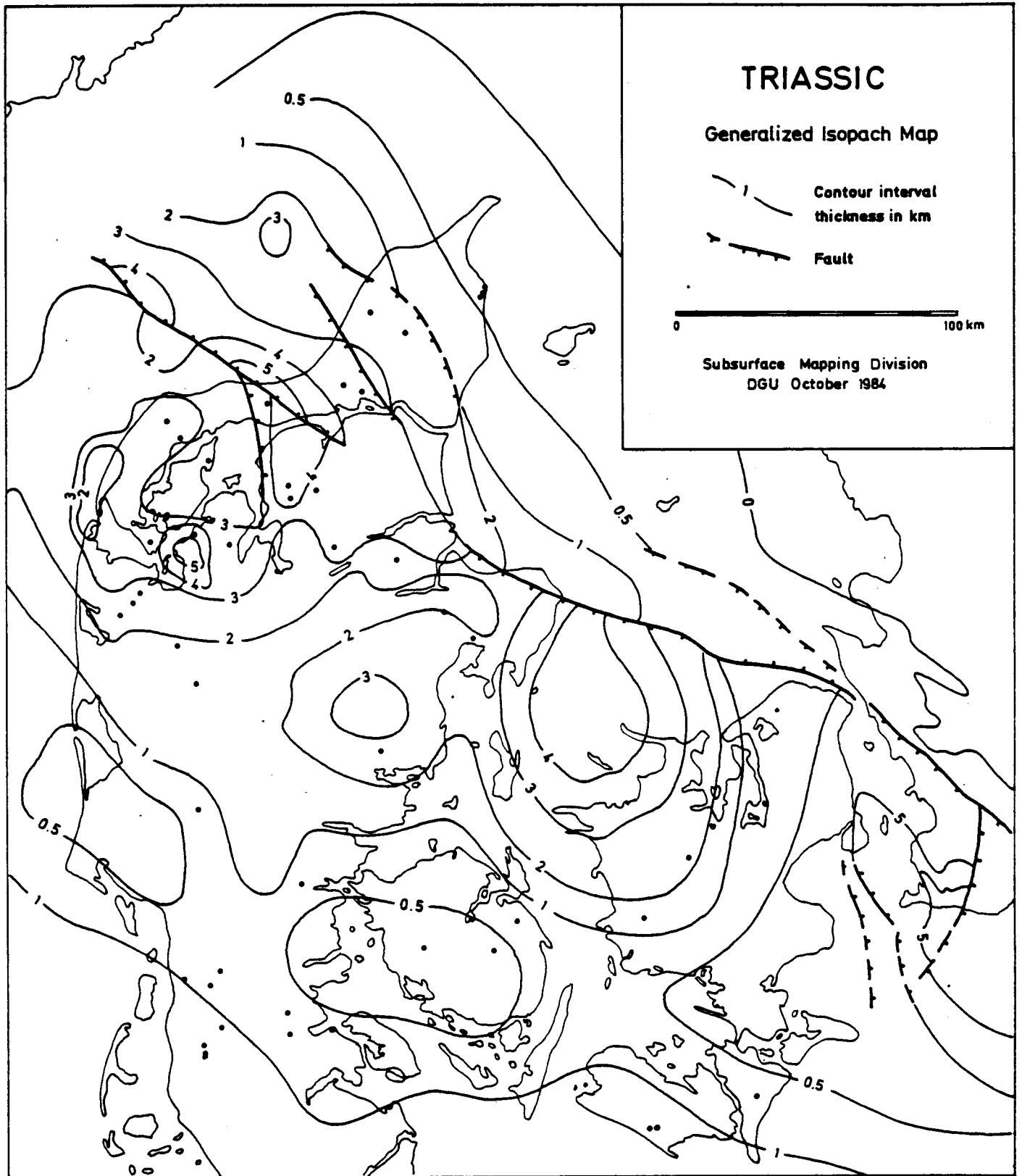


Fig.5

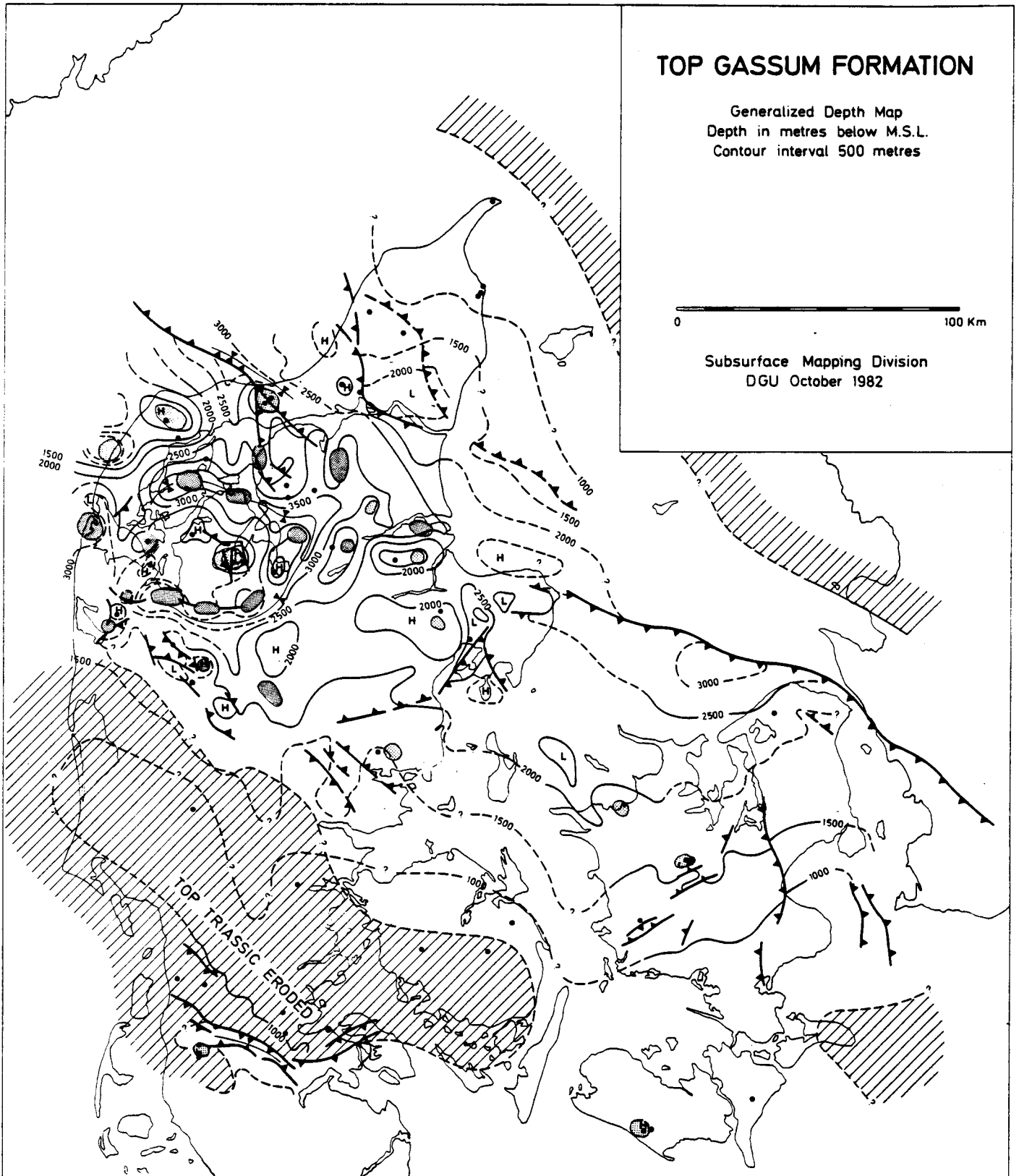


# TOP GASSUM FORMATION

Generalized Depth Map  
 Depth in metres below M.S.L.  
 Contour interval 500 metres

0 100 Km

Subsurface Mapping Division  
 DGU October 1982



**LEGEND:**

- |  |                           |   |  |
|--|---------------------------|---|--|
|  | Salt pillow               |   | Gassum Formation absent<br>(0 isopach) |
|  | Salt piercement           |   | Low trend                              |
|  | Fault (certain)           | H | High                                   |
|  | Fault (questionable)      | L | Low                                    |
|  | Depth contour             | • | Well site                              |
|  | Depth contour (uncertain) |   |  |

Fig.6

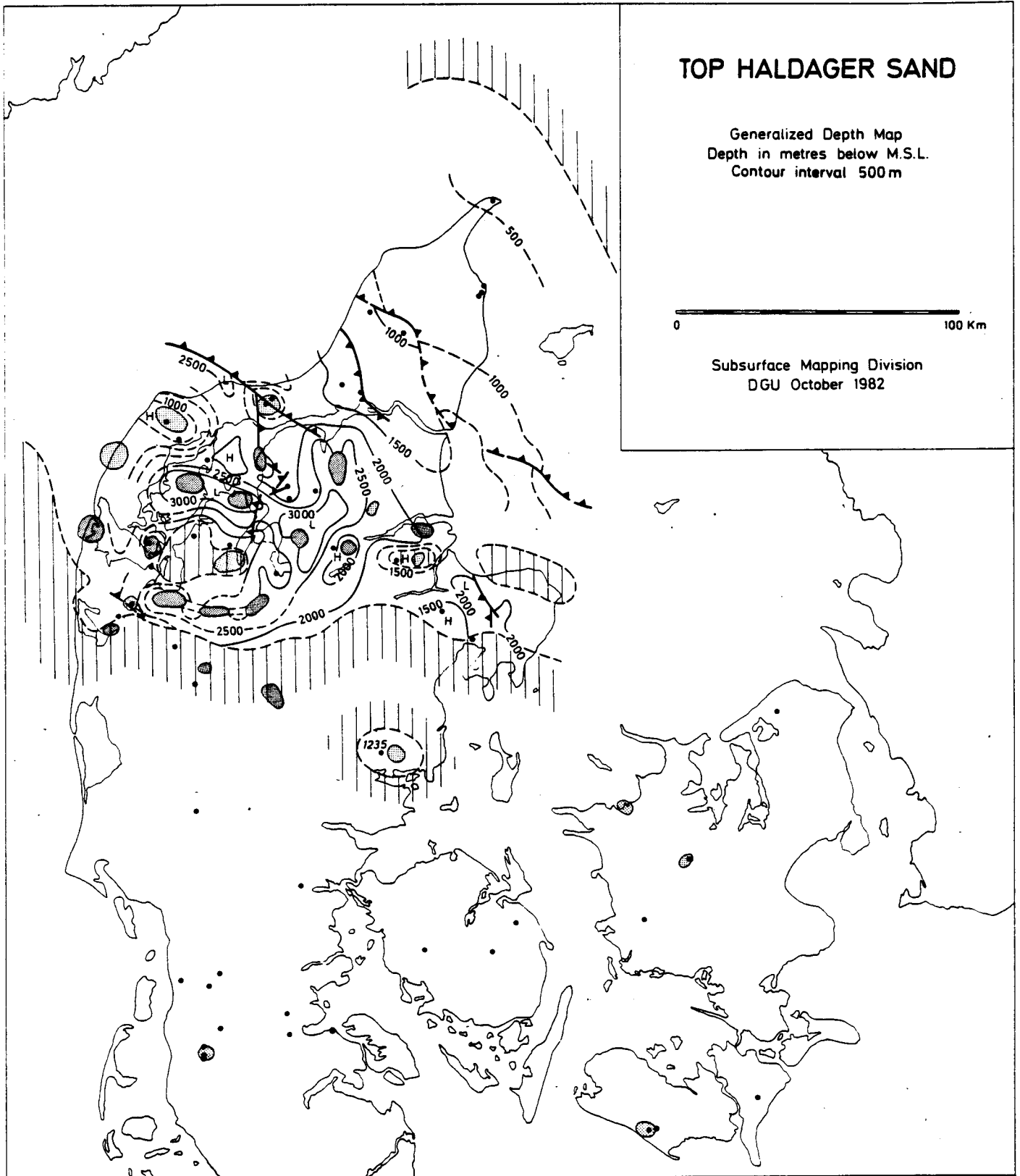


# TOP HALDAGER SAND

Generalized Depth Map  
 Depth in metres below M.S.L.  
 Contour interval 500 m

0 100 Km

Subsurface Mapping Division  
 DGU October 1982



## Legend:











- |   |                              |  |                           |
|---|------------------------------|--|---------------------------|
|  | Salt pillow                  |  | 1235 Depth from well data |
|  | Salt piercement              |  | Depth contour             |
|  | Fault (certain)              |  | Depth contour (uncertain) |
|  | Fault (questionable)         |   | High                      |
|  | Haldager Sand thin or absent |   | Low                       |

Fig.7



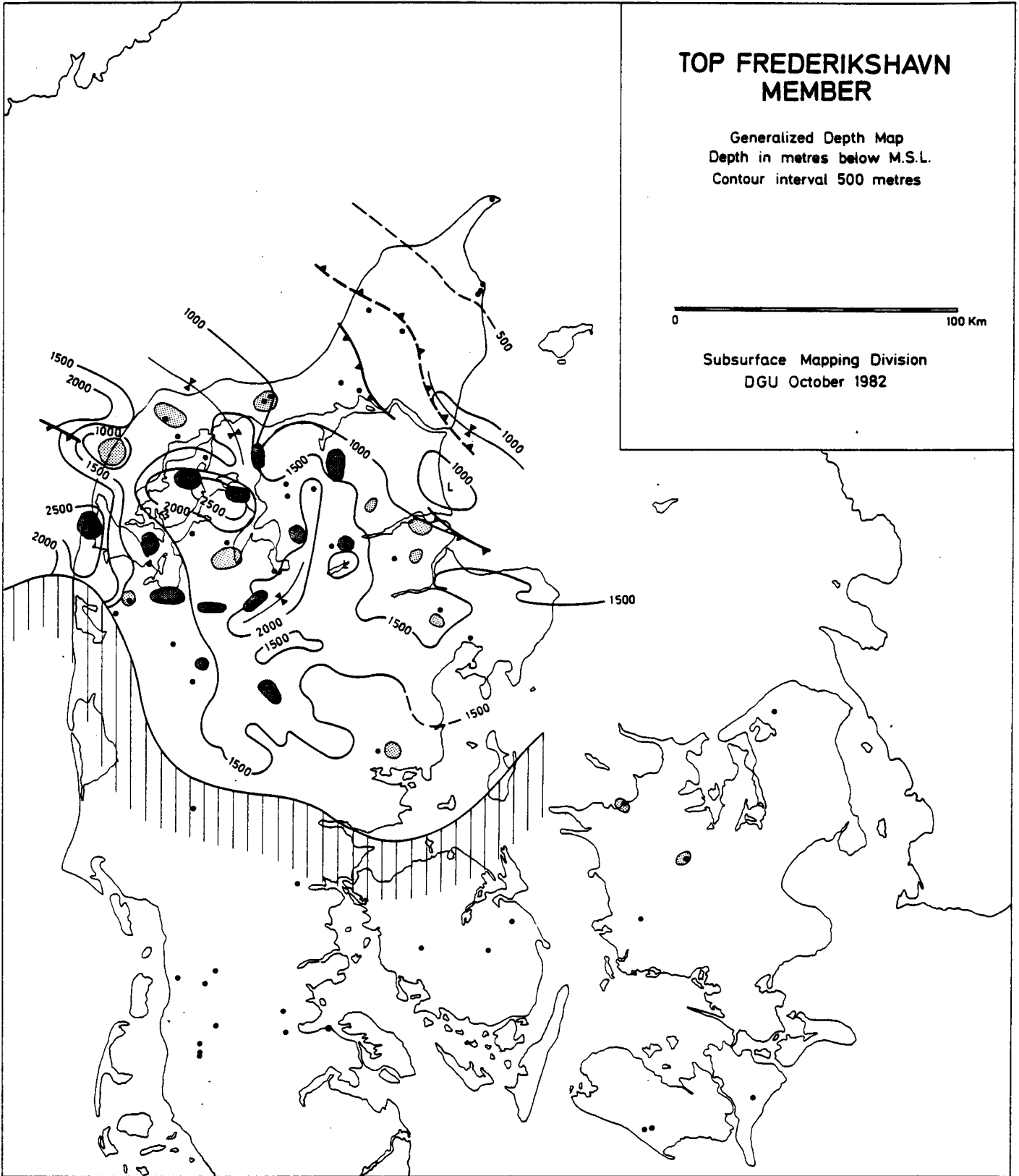


# TOP FREDERIKSHAVN MEMBER

Generalized Depth Map  
 Depth in metres below M.S.L.  
 Contour interval 500 metres

0 100 Km

Subsurface Mapping Division  
 DGU October 1982



**Legend:**

— Depth contour

- - - Depth contour (uncertain)

● Salt pillow

● Salt piercement

I Low trend

▨ Frederikshavn Member absent (0 isopach)

—▲ Fault (certain)

-▲- Fault (questionable)

H High

L Low

Fig.8



Fig. 9

POROSITY GRADIENTS FOR  
CLASTIC RESERVOIRS  
DGU NOVEMBER 1982

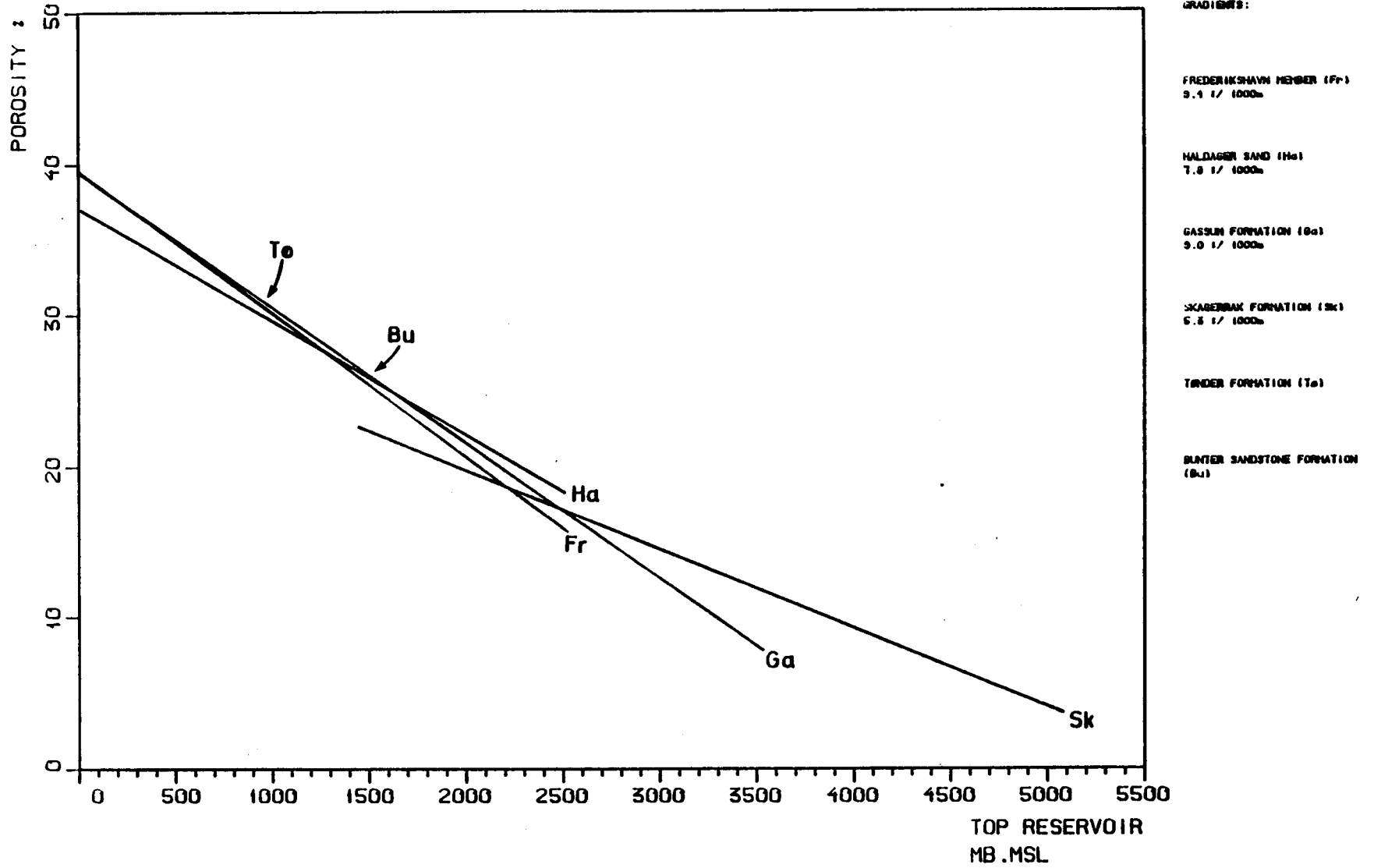
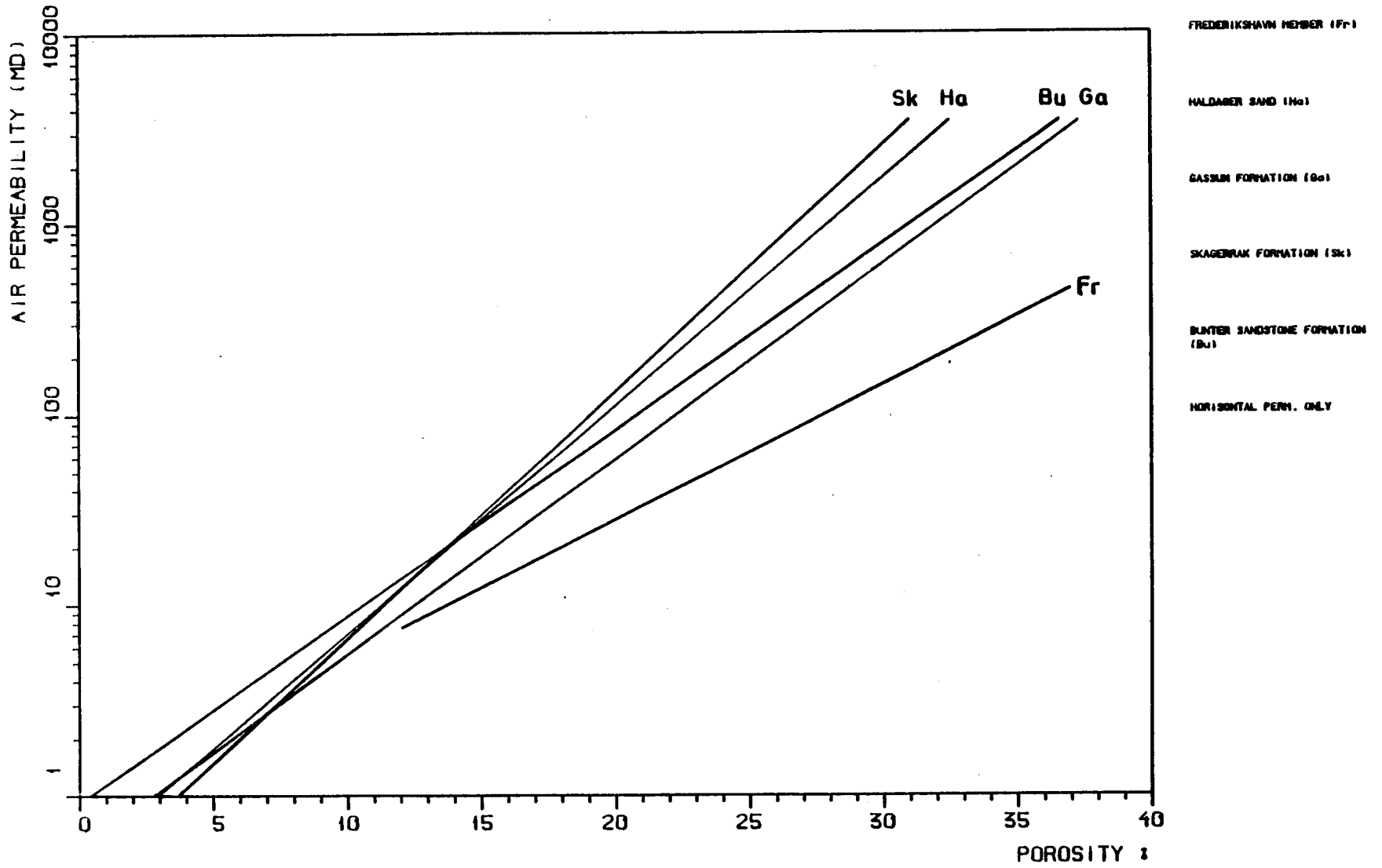


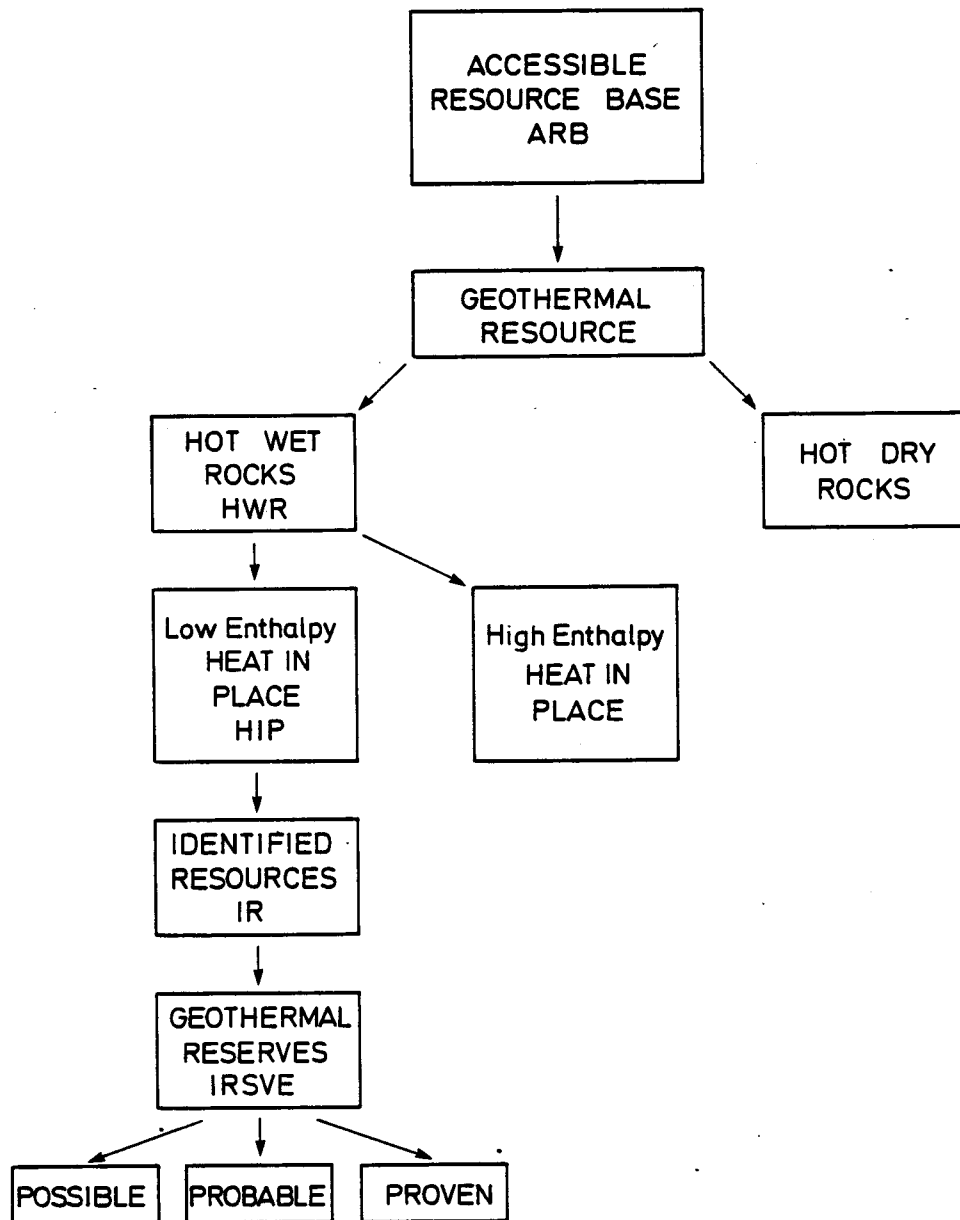


Fig.10

RELATIONSHIP BETWEEN POROSITY AND AIR PERMEABILITY  
FOR CLASTIC RESERVOIRS  
DGU NOVEMBER 1982





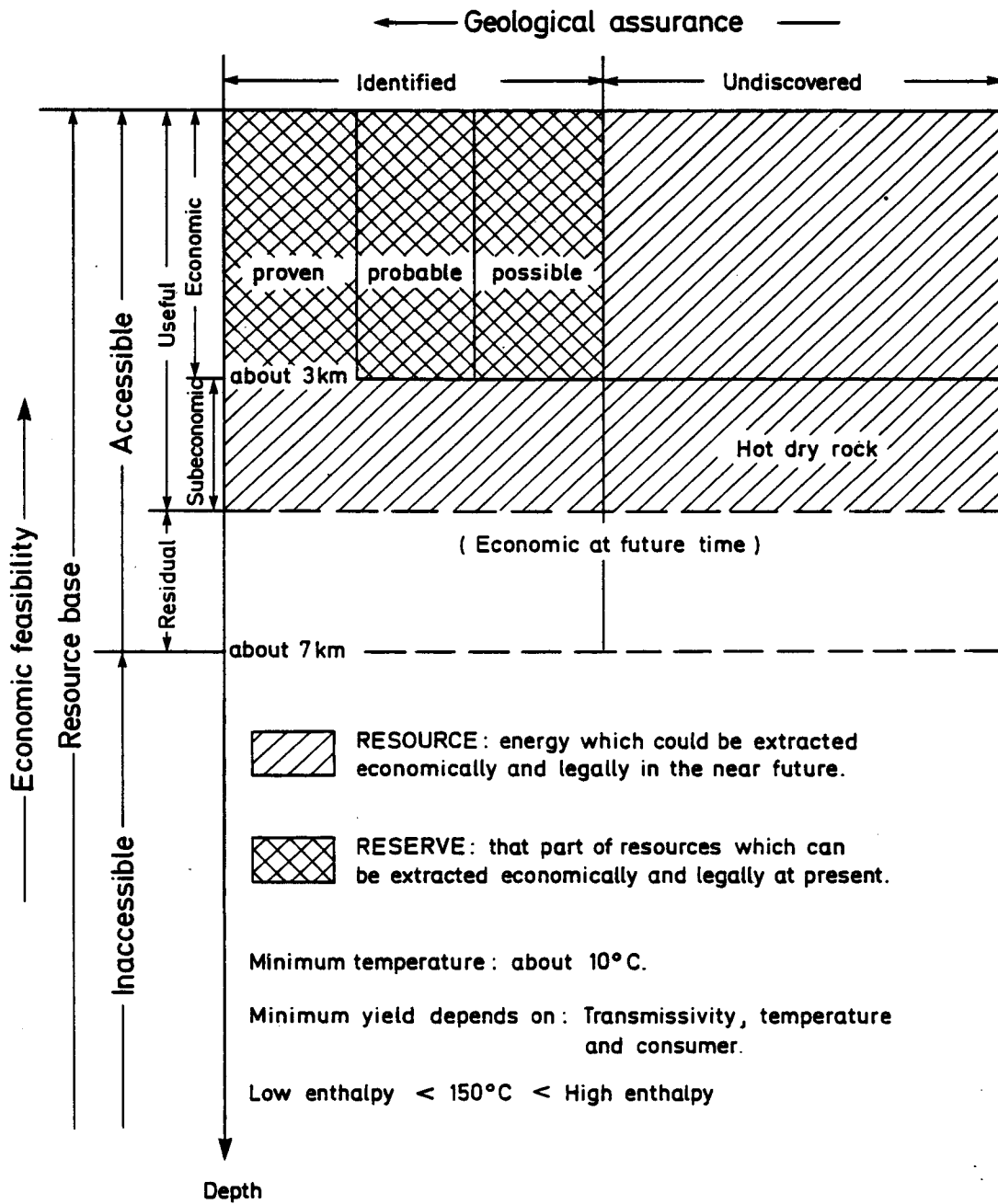


The evaluation procedure for resource and reserve assessment in the Danish sedimentary basins.

Fig.11







McKelvey diagram, revised version for geothermal energy

Modified after Muffler, L.J.P., and Marianne Guffanti, 1979. Assessment of geothermal resources of the United States 1978. - U.S. Geological Survey Circular 790, p. 1-7.



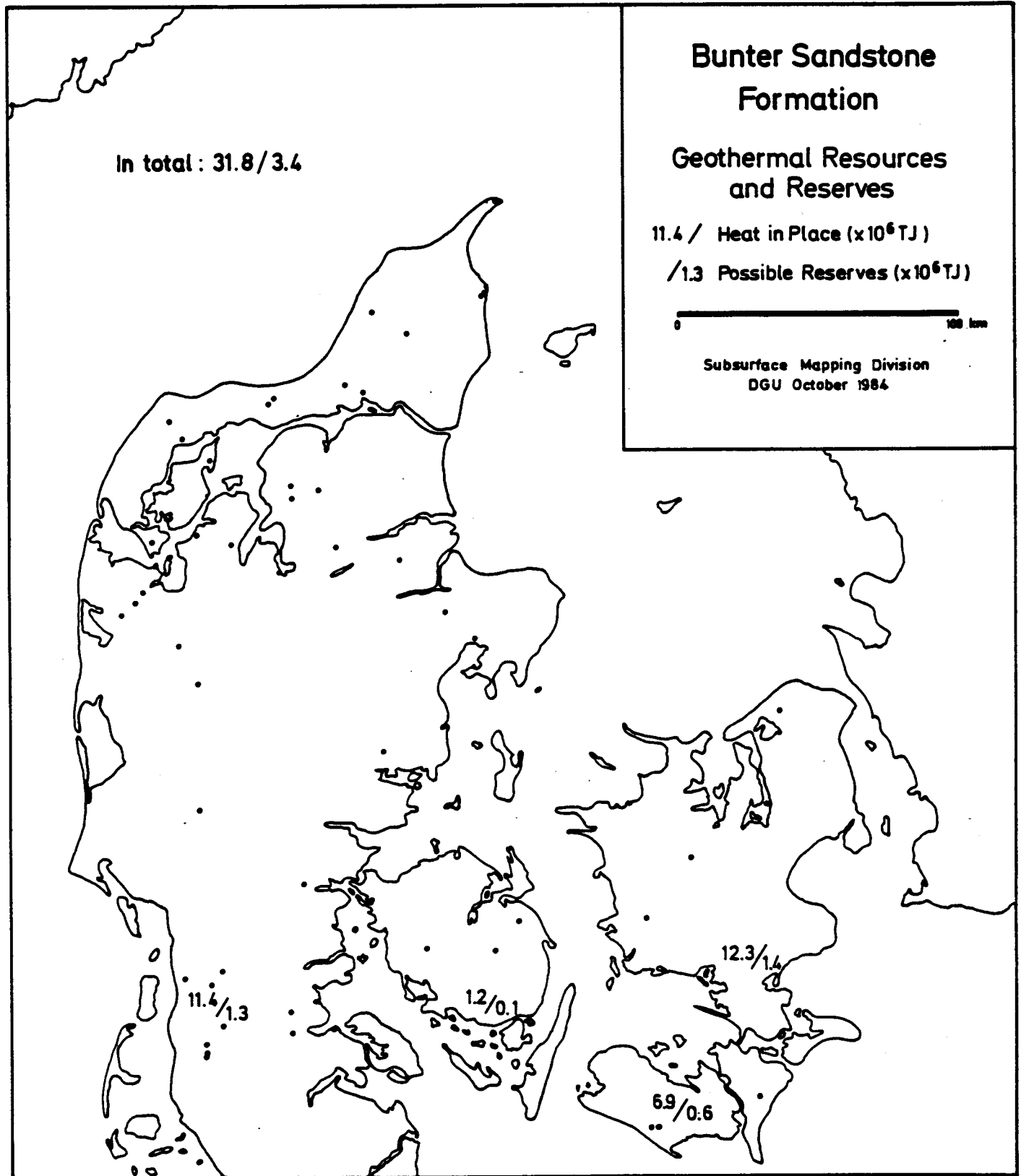


Fig.13



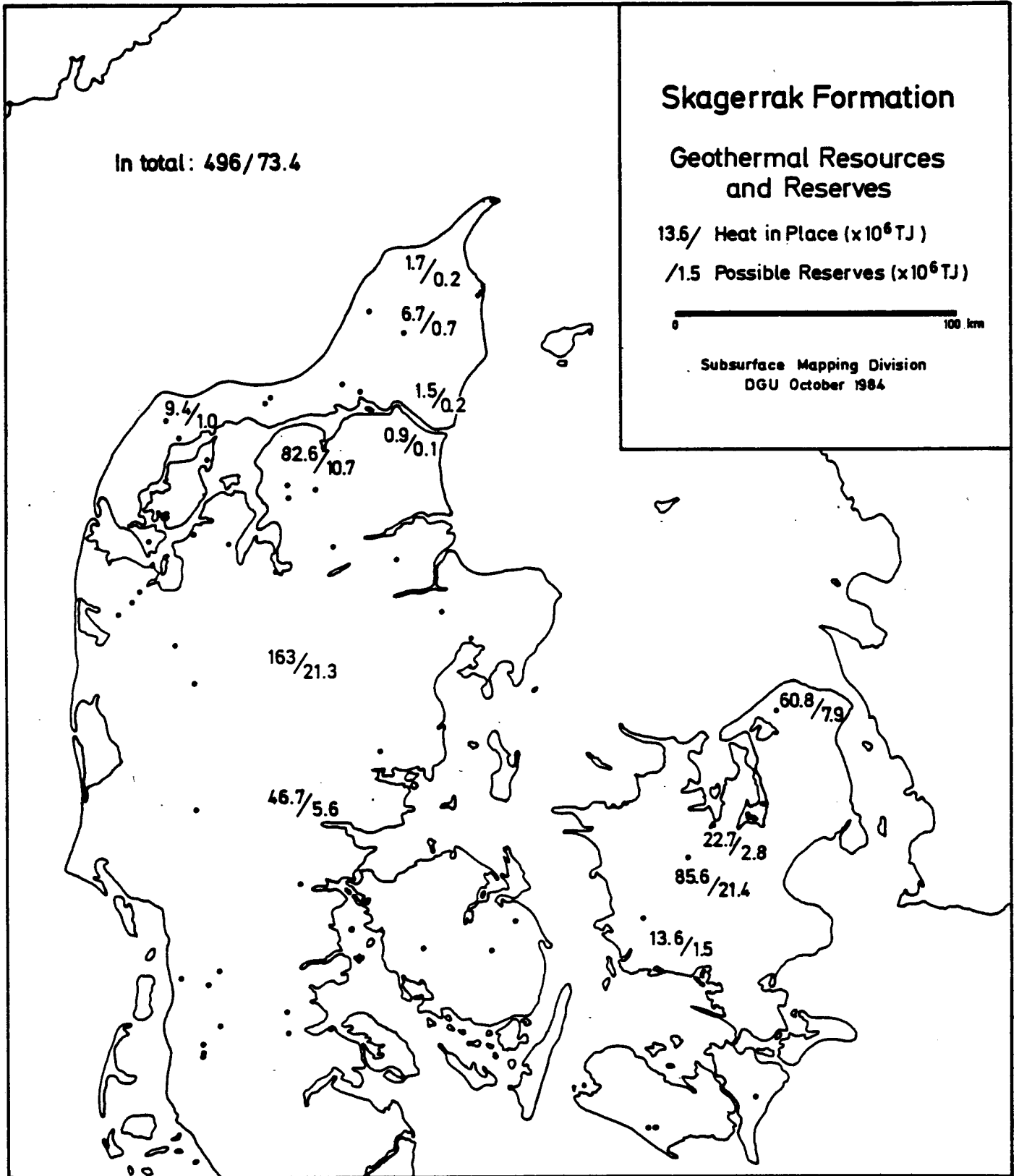


Fig.14



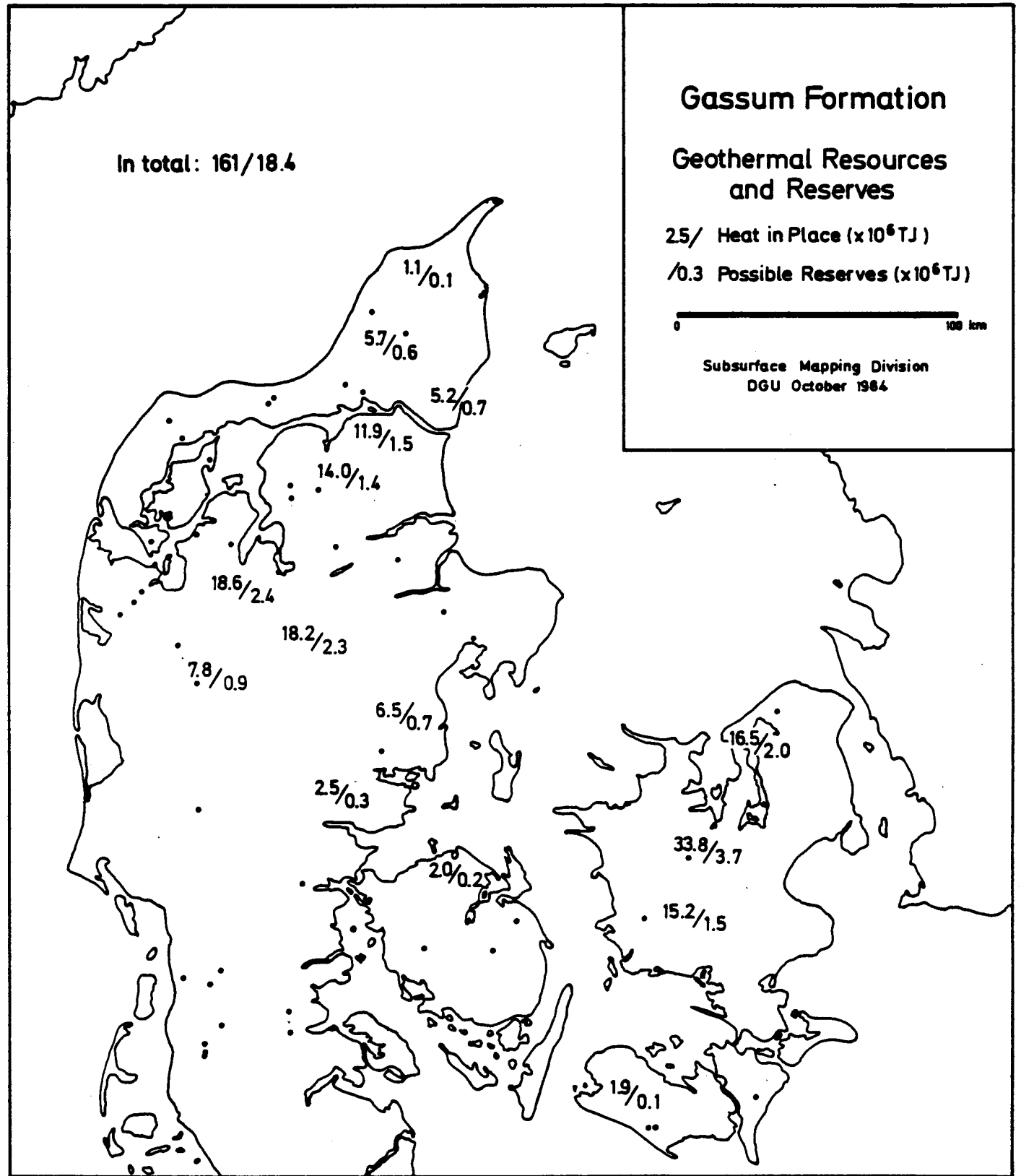


Fig.15





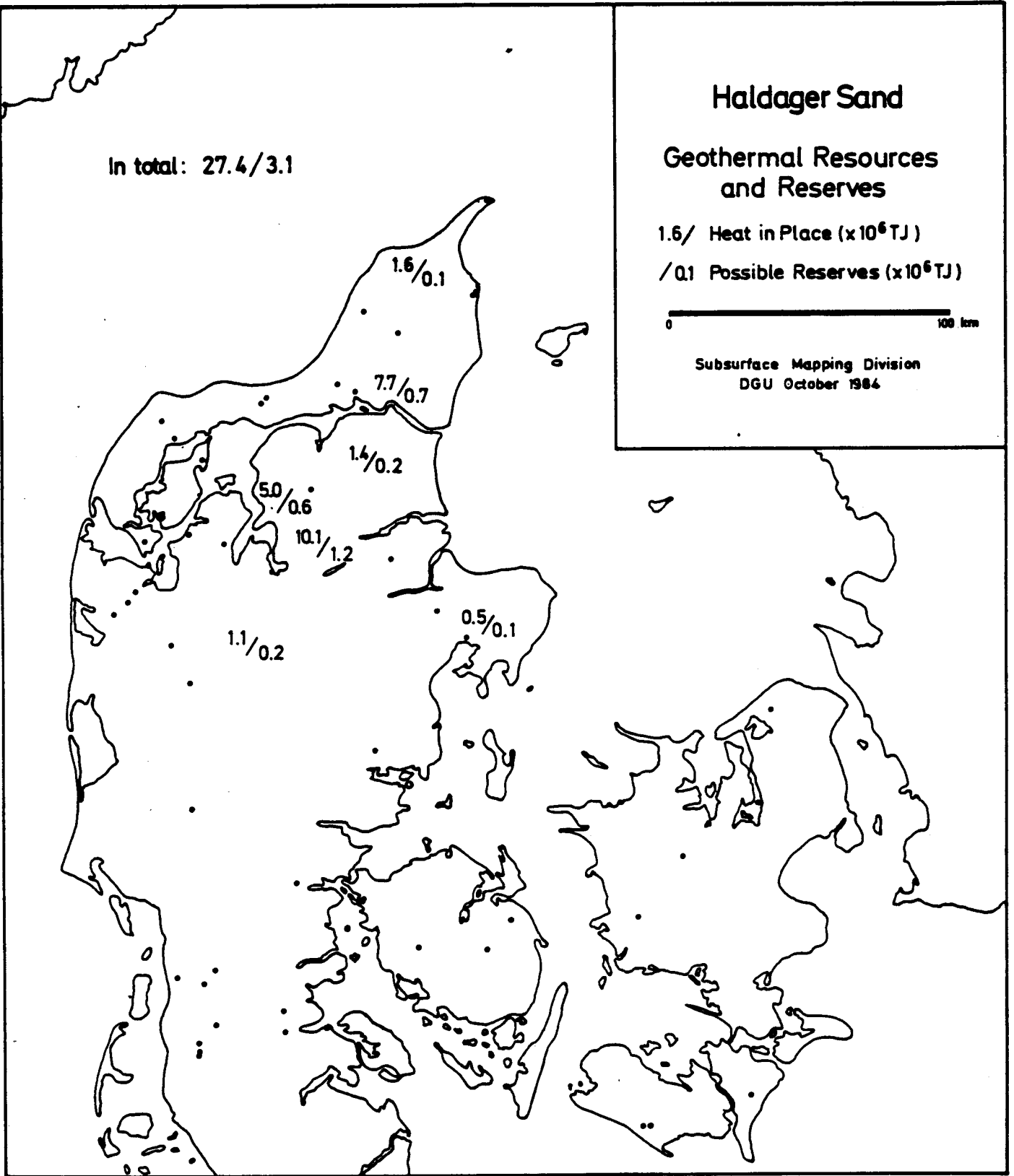


Fig.16



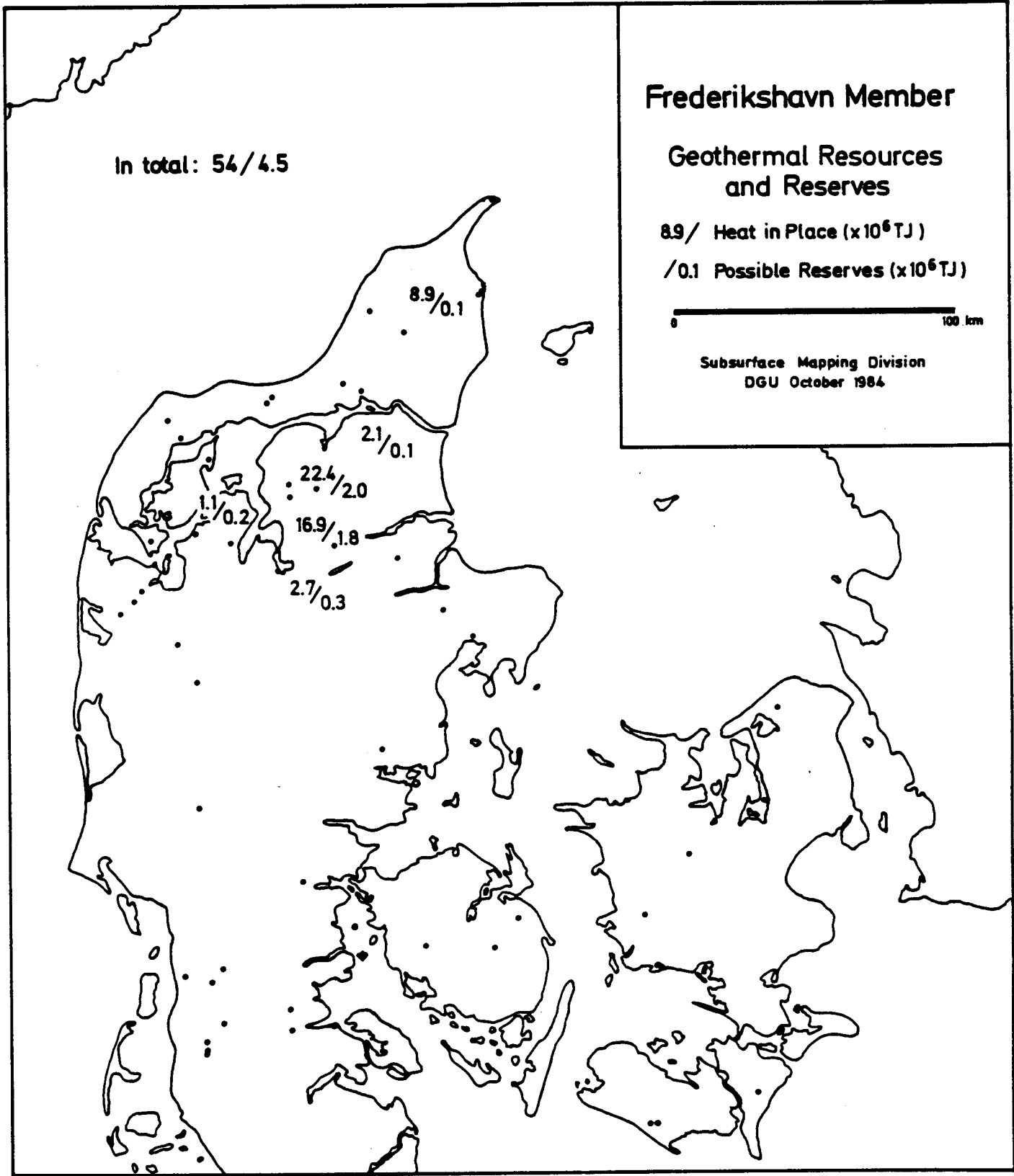
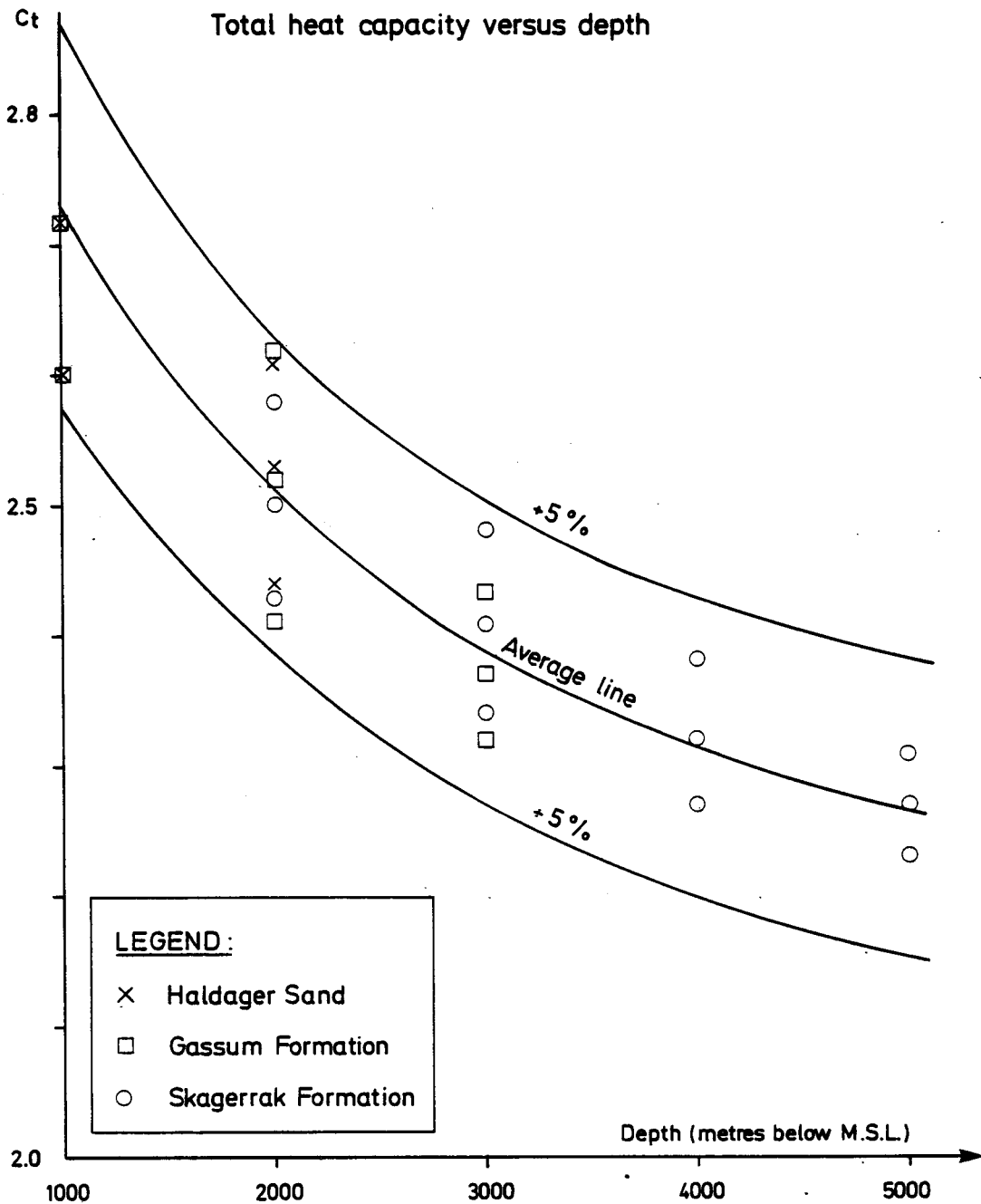


Fig.17

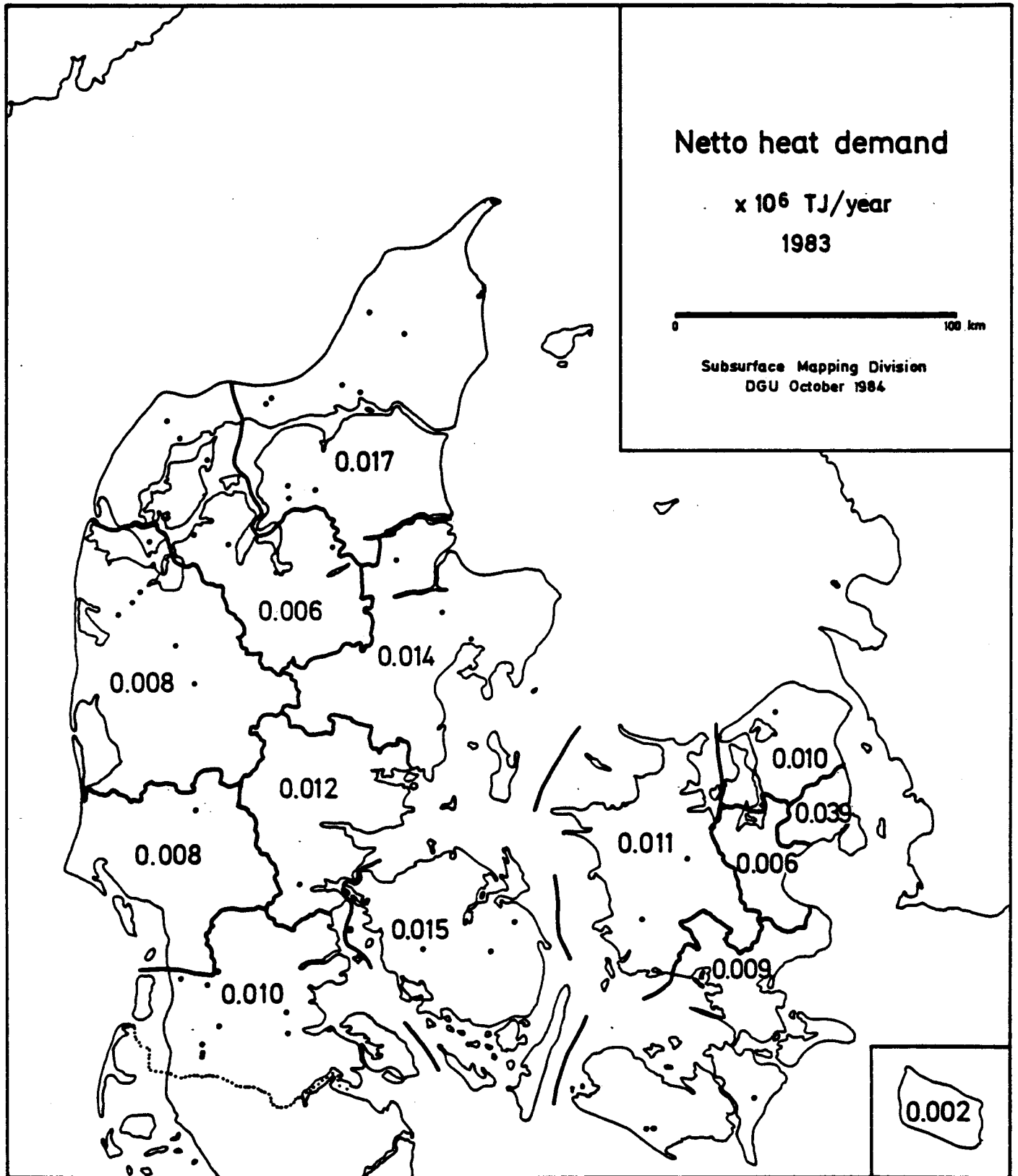




Total heat capacity,  $C_t$ , of Skagerrak Formation, Gassum Formation and Haldager Sand as a function of depth.  
 $C_t$  values based on table I.2. Personal communication from G. Iversen, D.O.N.G. A/S

Fig.18





Netto heat demand distributed on counties, x 10<sup>6</sup> TJ/year, 1983.  
 Based on Danish Energy Agency (DEA) working document, table III.1

Fig.19



The resources and reserves of low enthalpy geothermal energy sources in Denmark have been assessed.

A summary is given of the possible geothermal reservoirs with emphasis on their reservoir parameters and regional distributions. Based on these data the geothermal resources and reserves are presented.

The Accessible Resources Base, or the heat stored in the rocks and fluids, is found to be  $1.45 \times 10^6$  TJ/km<sup>2</sup> in the Danish Subbasin.

The Geothermal Resources, which is the heat in place stored in the reservoir volumes, is calculated to  $770 \times 10^6$  TJ.

The Identified Resources, representing the heat which can be produced, is found to be  $206 \times 10^6$  TJ.

The Identified Reserves, the energy output when exploiting the Identified Resources, is estimated to be  $103 \times 10^6$  TJ; of this, about  $67 \times 10^6$  TJ is considered possible to exploit economically. To put these figures in relief, the total heat demand in Denmark is about  $0.17 \times 10^6$  TJ per year.

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